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L171 CL-80 CY6250B X 2000

OPERATION INSTRUCTION

09-12-2002

Contents

I.	Applications	1-2
II.	Specifications	3-6
III.	Slings, handling and installation	6-7
IV.	Operating system	8-12
V.	Drive system	13-20
VI.	Electrical system	21-24
VII.	Lubricating system	25-28
VIII.	Cooling system	28
IX.	Construction and adjustment	29-39
X.	Maintenance and service	40-41
XI.	Attachments and tools	42-50
XII.	Easy worn parts and their drawings	51-60
	Spare Parts	

Important

To avoid any misunderstanding, when ordering spare parts or easy worn parts please always mention on your order:

- 1) The machine serial number;
- 2) The parts number on page 13 for spare parts.

The parts number on page 41 for easy worn parts.

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产品型号	
文件代号	SY-AG-7
第 2 页	共 61 页

This operating instruction booklet is applicable to the following models CY6140B and CY6150B as well as Universal Lathes of models CY6240B and CY6250B.

I. Applications

On ferrous or non-ferrous metals, plastics or synthetic rubber workpieces can these Universal Lathes, either used in roughing or finishing, perform all basic turning operations, such as external and internal cylindrical, conical or any kind of rotary surfaces, end-facing, grooving, cutting-off as well as thread-cutting in inch, metric, diametral pitch and module, including drilling, reaming, knurling and oil-groove broaching etc.

These lathes are built to a high degree of working accuracy with roundness error within 0.01mm, cylindricity error within 0.01mm on measured length of 100mm, the surface finish is not less than $\sqrt{6}$ and threadpitch error within 0.06mm on measured length of 300mm. Lathes of CY6140B and CY6150B as well as CY6240B and CY6250B are then suitable for production and maintenance operations in single job and small batch works in machine shops, toolrooms, maintenance depots and laboratories.

We hope that through this booklet of "Operating Instruction" the machines will be properly installed. With ordinary care in service and periodical inspection on levelling, they will maintain their original accuracy for many years.

产品型号		第 3 页
文件代号	5Y-A5-7	共 61 页
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Specifications

A. Capacity

	Model	CY6110B	CY6240B	CY6150B	
1. Swing over bed	mm	400	400	500	500
2. Swing over cross slide	mm	220	220	300	300
3. Swing in gap	mm		630		710
4. Effective length in gap	mm		240		240
5. Max. center distance	mm	750,	1000,	1500,	2000.
6. Spindle thru-bore diameter	mm	82			

B. Main spindle

1. Spindle nose-camlock, short-taper flange type D - 8
2. Spindle taper bore: taper and diameter 1:20; 90mm
3. Number of speeds 24
4. Range of speeds 9-1600 r/min

C. Feeds and threads

1. Steps and range of feeds

- Basic feeds: 65 longitudinal feeds 0.063 to 2.52 mm/r
 65 transversal feeds 0.025 to 1.01 mm/r
- Reduced feeds: 13 longitudinal feeds 0.028 to 0.056 mm/r
 13 transversal feeds 0.011 to 0.023 mm/r
- Amplified feeds: 15 longitudinal feeds 2.86 to 6.43 mm/r
 15 transversal feeds 1.15 to 2.58 mm/r

2. Rapid travelling speeds: longitudinal 4.5 m/min (50Hz) or 5.4 m/min (60Hz) transversal 1.9 m/min (50Hz) or 2.3 m/min (60Hz)

3. Varieties, steps and range of threads

- | | |
|----------------------------|--------------------|
| 48 inch threads | 72 to 1/8 teeth/in |
| 48 metric threads | 0.5 to 224 mm |
| 45 diametral pitch threads | 56 to 1/4 DP |
| 42 module threads | 0.5 to 112 mm |
| Pitch of leadcrew | 12 mm |

D. Carriage

1. Distance from tool-supporting base in tool post to main spindle axis 28 mm
2. Max. cross section of tool chock 25 mm X 25 mm
3. Graduation in degrees on swivel base
clockwise 45° and counterclockwise 135°

品型号	文件代号	SY-AB-R
图号	图名	
比例	日期	

- 4. Max. travel of top slide 145 mm
- 5. Max. travel of cross slide, for CY6140B and CY6240B: 320 mm
for CY6150B and CY6250B: 340 mm
- 6. Permissible max. cutting force P_z 13700 N
- 7. Permissible max. feeding force P_x 3400 N

E. Tailstock

- 1. Tailstock quill diameter 75 mm
- 2. Max. travel of tailstock quill 150 mm
- 3. Tailstock center taper 5 MT
- 4. Max. set-over of tailstock ± 15 mm

F. Motors and V-Belts

- 1. Power mains: AC Frequency 50Hz or 60Hz
Voltage 220V, 380V, 420V or 440V
- 2. Main drive motor: Type 132M-4 7.5KW
Type 160M-4 11 KW
Type 160L-4 15 KW
- 3. Rapid travel motor: Type 2AOS 5634, 250 W
- 4. Coolant pump motor: Type AOB--25, 60 W
flow capacity 25 l/min
- 5. V-Belts for main drive motor:
B--2210, 4pcs for CY6140B and CY6240B with motor y132
B--2184, 4pcs for CY6140B and CY6240B with motor y160
B--2286, 4pcs for CY6150B and CY6250B with motor y132
B--2261, 4pcs for CY6150B and CY6250B with motor y160

J. Overall dimensions and net weight

Model	Max. center distance mm	Overall dimensions (L x W x H) mm	Net weight Kg
CY6140B	750	2375 x 1043 x 1275	2175
	1000	2625 x 1043 x 1275	2250
CY6240B	1500	3125 x 1043 x 1275	2450
	2000	3625 x 1043 x 1275	2650
CY6150B	750	2375 x 1077 x 1315	2250
	1000	2625 x 1077 x 1315	2300
CY6250B	1500	3125 x 1077 x 1315	2500
	2000	3625 x 1077 x 1315	2700

编 号
 文件代号 SY-AB-7
 日期
 共 1 / 1
 第 5

Max center distance	750	1000	1500	2000
A	875	1125	1625	2055 + 660 + 610
B	1305	1555	2055	1205 + 1270

Model	CY6140B	CY6150E
C	CY6240B	CY6250D
	578	513

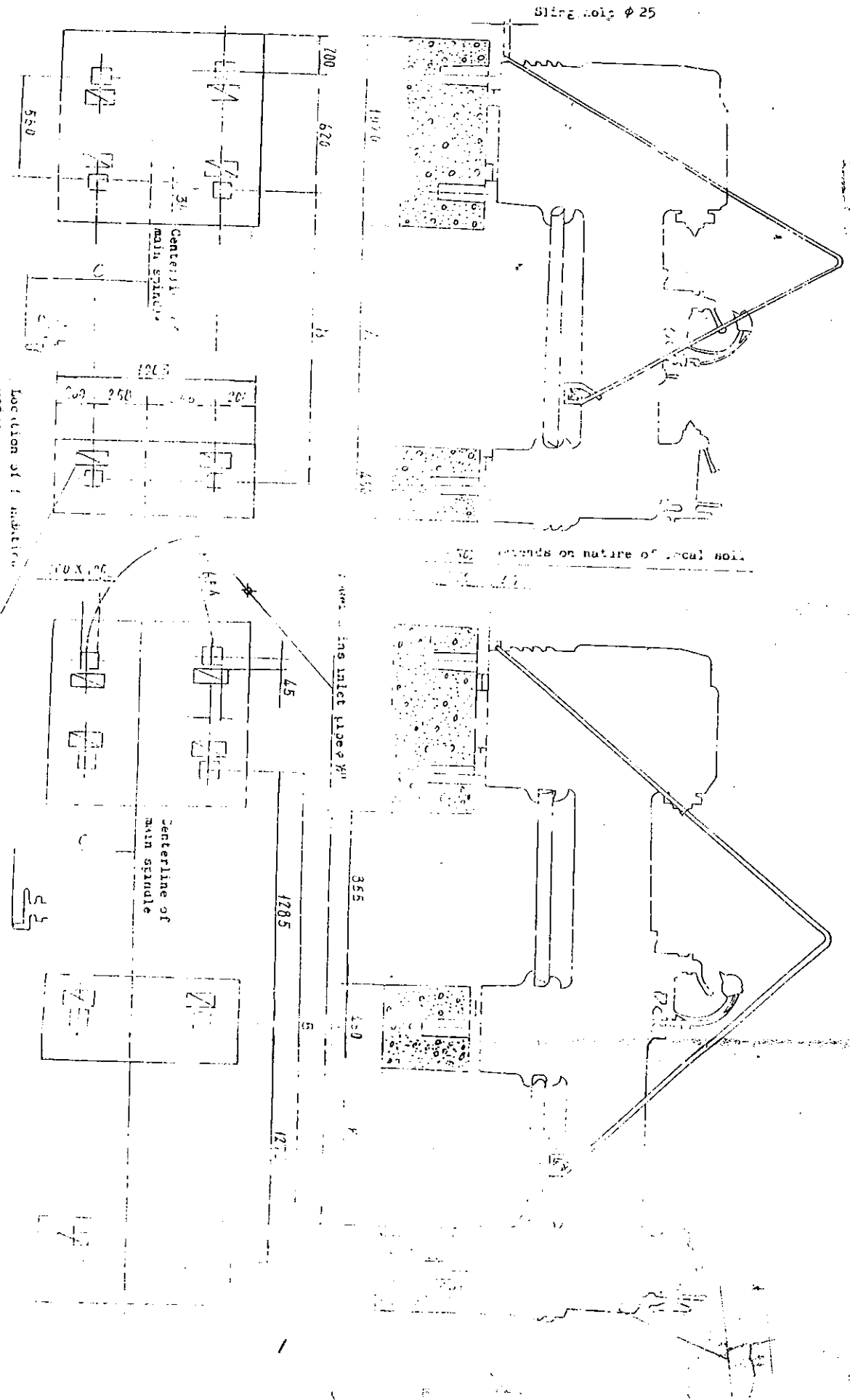


Fig. 1 Slinging and foundation plan

III. Slings, handling and installation

(A) Slings and handling

When lifting the packed lathe, ropes must be slung in accordance with the marks on the packing case. In transporting and unloading don't let it too much be tilted and the case should not be percussed or shocked violently so as not to damage the casebottom or the sideplates. Placing the case on edged bodies or upside down is strictly forbidden.

After the case is opened, inspect the outward condition of the machine immediately and check up the accessories and tools according to the packing list.

Follow the arrangements shown in Fig.1 to lift the lathe after unpacking. Depending upon the length of bed, the machine can be balanced by moving the saddle longitudinally to distribute the weight equally about the sling. Put soft pads or felt between ropes and the painted surface of lathe and care must be taken not to catch any of the levers or pushbuttons with the ropes when lifting.

(B) Installation

The machine has been checked and tested before delivery, yet installation should be carried out correctly to insure the machining accuracy for long time.

As shown in Fig.1 the lathe is supported on preconcreted base by a number of foundation wedges. Adjust the wedges by using a precision level to keep the longitudinal level not over 0.04 mm per meter and the transverse level not over 0.03/1000 mm

Whenever an approximate levelling is being finished, fill up the foundation bolt housings with concrete to fix the bolts. After it is fully dry and hardened, then carry on an accurate levelling, adjust the wedges gradually and tighten up the foundation bolt nuts evenly until the accurate levelling is obtained. Finally pour cement between the ground and the base to fix the foundation wedges, seal the surrounding area of the cabinet legs and smooth the ground surface.

Recheck the levelling once more before using the machine. Afterwards, every three months a periodical levelling check is necessary.

(C) Cleaning

Carefully remove the anti-corrosion coatings on all parts with kerosene. Wash the inner part of the headstock with heated kerosene. All capillary woolen yarns must be cleaned attentively one by one. Smear the sliding guide ways, leadscrew, feed shaft etc, with machine oil after washing and cleaning. When all parts of the machine are cleaned thoroughly and perfectly, then give a general lubrication sufficiently according to the lubricating system diagram.

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Before putting the machine into operation, the operator should read through every section of the manual, understand the construction of the machine and acquaint himself with the position of all the operating parts and the details of operation.

Check the oiling condition of all the lubricating points.

Check the working condition of each part of the machine manually.

Before power is supplied, check the electrical system to make sure that the system is in good condition and whether motor is damped. After power is supplied, check whether the main motor is rotating in clockwise direction (left view from the motor), if not, correct the electric connection immediately.

The above check being accomplished, a trial running test will be carried out. In the beginning of the trial the machine must be run at a minimum speed for some time and then gradually be accelerated. While the machine is running check the lubricating, electrical and cooling system as well as the operating condition of each part attentively.

Only when the machine is normally operating, well-lubricating, well-cooled, manipulating and sensitively braking, can it be started to work.

产品型号	
文件代号	SY-AB-t
第 8	共 61

1. Pushbutton control of coolant pump
2. Pushbutton control of main drive motor
3. Pushbutton control of main drive motor
4. Pulley and drive lever
5. Manual and automatic pitches, control of reverse feed lever
6. Feed rate control dial knob
7. Feedback lever for ratio change lever
8. Main spindle speed change lever
9. Forward and reverse gear change lever

10. Main spindle speed change lever
11. Main spindle forward-brake-reverse lever
12. Pushbutton control of main motor
13. Split-out clamping and releasing lever
14. Cross slide traverse ball crank handle
15. Square turret cramping clamping handle
16. Lamp switch
17. Saddle longitudinal travel handwheel
18. Lock screw of saddle

19. Main spindle forward-brake-reverse lever
20. Four-way power-feed lever with rapid-travel pushbutton
21. Top slide travel lever
22. Coolant flow regulating cock
23. Quill clamping handle
24. Tailstock clamping handle
25. Quill travel handwheel

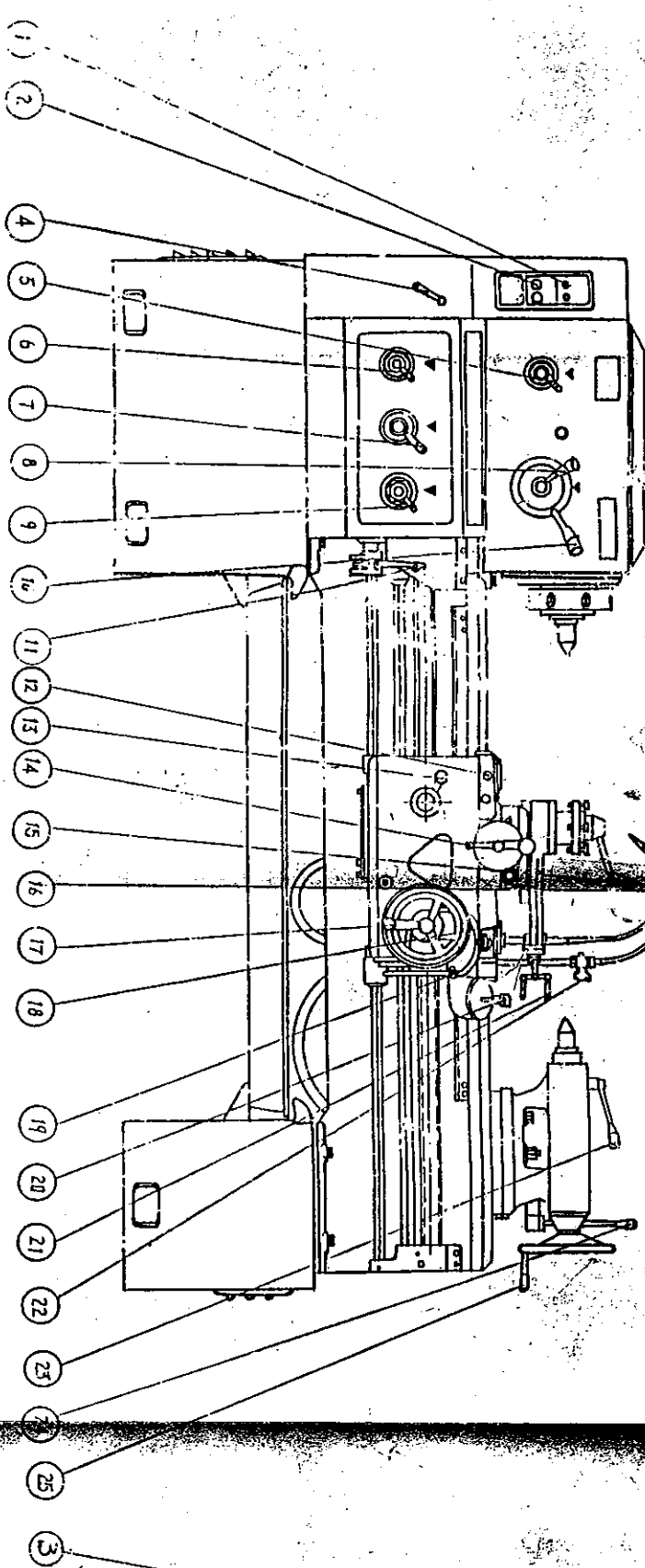


Fig. 2 Operating elements and their locations

TYPE CY6240B

Table 2 Feedrates and Threadpitches

n	mm				mm				mm			
	A	B	C	D	A	B	C	D	A	B	C	D
0.028	0.09	0.10	0.36	0.71	2.86	0.012	0.027	0.040	0.076	0.15	0.30	1.21
0.031	0.10	0.20	0.40	0.60	3.21	0.013	0.030	0.043	0.085	0.17	0.34	1.36
0.033	0.10	0.21	0.42	0.63	3.33	0.014	0.031	0.044	0.089	0.18	0.35	1.42
0.035	0.11	0.22	0.44	0.69	3.57	0.015	0.033	0.047	0.095	0.19	0.38	1.52
0.041	0.11	0.23	0.46	0.92	3.57	0.016	0.034	0.047	0.095	0.19	0.38	1.52
0.037	0.084	0.12	0.24	0.48	3.00	0.016	0.036	0.050	0.101	0.20	0.40	1.62
0.038	0.087	0.13	0.25	0.49	3.92	0.017	0.037	0.052	0.104	0.21	0.42	1.67
0.042	0.13	0.27	0.53	1.07	4.28	0.018	0.038	0.053	0.106	0.21	0.42	1.67
0.046	0.14	0.29	0.58	1.17	4.67	0.019	0.040	0.055	0.111	0.22	0.44	1.82
0.047	0.15	0.30	0.60	1.21	4.82	0.020	0.041	0.056	0.113	0.22	0.44	1.82
0.049	0.15	0.31	0.62	1.25	5.00	0.021	0.042	0.057	0.114	0.23	0.46	1.89
0.050	0.16	0.32	0.64	1.29	5.16	0.021	0.043	0.058	0.116	0.23	0.46	1.89
0.054	0.17	0.34	0.68	1.38	5.51	0.023	0.045	0.061	0.121	0.24	0.48	2.05
0.056	0.17	0.35	0.70	1.43	5.71	0.024	0.046	0.062	0.122	0.24	0.48	2.05
				1.61	6.43	0.026						2.12
												2.19
												2.34
												2.43
												2.73

n	mm				mm				mm				DP	DP/1/π	n	
	A	B	C	D	A	B	C	D	A	B	C	D				
1	2	4	8	16	32	64	128	256	512	1024	2048	4096	8192	16384	32768	65536
2	0.5	1.0	2.0	4.0	8.0	16.0	32.0	64.0	128.0	256.0	512.0	1024.0	2048.0	4096.0	8192.0	16384.0
3	0.5	1.0	2.0	4.0	8.0	16.0	32.0	64.0	128.0	256.0	512.0	1024.0	2048.0	4096.0	8192.0	16384.0
4	1.25	2.5	5.0	10.0	20.0	40.0	80.0	160.0	320.0	640.0	1280.0	2560.0	5120.0	10240.0	20480.0	40960.0
5	1.25	2.5	5.0	10.0	20.0	40.0	80.0	160.0	320.0	640.0	1280.0	2560.0	5120.0	10240.0	20480.0	40960.0
6	1.25	2.5	5.0	10.0	20.0	40.0	80.0	160.0	320.0	640.0	1280.0	2560.0	5120.0	10240.0	20480.0	40960.0
7	2.75	5.5	11.0	22.0	44.0	88.0	176.0	352.0	704.0	1408.0	2816.0	5632.0	11264.0	22528.0	45056.0	90112.0
8	1.5	3.0	6.0	12.0	24.0	48.0	96.0	192.0	384.0	768.0	1536.0	3072.0	6144.0	12288.0	24576.0	49152.0
9	1.5	3.0	6.0	12.0	24.0	48.0	96.0	192.0	384.0	768.0	1536.0	3072.0	6144.0	12288.0	24576.0	49152.0
10	0.75	1.5	3.0	6.0	12.0	24.0	48.0	96.0	192.0	384.0	768.0	1536.0	3072.0	6144.0	12288.0	24576.0
11	1.75	3.5	7.0	14.0	28.0	56.0	112.0	224.0	448.0	896.0	1792.0	3584.0	7168.0	14336.0	28672.0	57344.0
12	1.75	3.5	7.0	14.0	28.0	56.0	112.0	224.0	448.0	896.0	1792.0	3584.0	7168.0	14336.0	28672.0	57344.0
13	1.75	3.5	7.0	14.0	28.0	56.0	112.0	224.0	448.0	896.0	1792.0	3584.0	7168.0	14336.0	28672.0	57344.0
14	1.75	3.5	7.0	14.0	28.0	56.0	112.0	224.0	448.0	896.0	1792.0	3584.0	7168.0	14336.0	28672.0	57344.0
15	1.75	3.5	7.0	14.0	28.0	56.0	112.0	224.0	448.0	896.0	1792.0	3584.0	7168.0	14336.0	28672.0	57344.0

TYPE: CY62508

Table 2 Feedrates and Threadpitches

n	mm				mm				mm				
	t	A	B	C	t	A	B	C	t	A	B	C	
0.028	0.053	0.09	0.15	0.36	0.71	2.06	0.012	0.027	0.040	0.076	0.151	0.30	1.21
0.031	0.070	0.10	0.20	0.40	0.80	3.21	0.013	0.030	0.043	0.085	0.17	0.34	1.36
0.033	0.073	0.21	0.42	0.83	1.66	3.33	0.014	0.031	0.044	0.089	0.18	0.35	1.42
0.035	0.079	0.11	0.22	0.44	0.89	3.57	0.015	0.033	0.047	0.095	0.19	0.38	1.52
0.081	0.16	0.23	0.46	0.92	1.84	3.67	0.034	0.071	0.102	0.20	0.40	0.80	3.16
0.057	0.064	0.12	0.24	0.48	0.95	3.86	0.016	0.036	0.050	0.101	0.20	0.40	1.62
0.038	0.087	0.25	0.49	0.98	1.96	3.97	0.017	0.037	0.052	0.104	0.21	0.42	1.67
0.042	0.13	0.27	0.53	1.07	2.14	4.20	0.018	0.038	0.053	0.106	0.21	0.42	1.82
0.046	0.14	0.29	0.58	1.17	2.34	4.67	0.019	0.041	0.057	0.114	0.23	0.46	1.82
0.047	0.15	0.30	0.60	1.21	2.42	4.82	0.020	0.042	0.058	0.116	0.23	0.46	1.99
0.049	0.31	0.62	1.25	2.50	5.00	5.00	0.021	0.043	0.060	0.120	0.25	0.51	2.05
0.050	0.16	0.32	0.64	1.29	2.58	5.16	0.021	0.044	0.061	0.122	0.25	0.51	2.12
0.054	0.17	0.34	0.68	1.36	2.72	5.44	0.023	0.046	0.063	0.127	0.27	0.55	2.19
0.056	0.17	0.34	0.68	1.36	2.72	5.44	0.023	0.046	0.063	0.127	0.27	0.55	2.34
													2.43
													2.53
													2.68
													2.73

I	mm				mm				mm				
	t	A	B	C	t	A	B	C	t	A	B	C	
1	1	2	4	8	16	32	64	128	0.5	1	2	4	8
2	0.5	2.25	4.5	9	18	36	72	144	2.25	4.5	9	18	36
3													
4	1.25	2.5	5	10	20	40	80	160	1.25	2.5	5	10	20
5													
6													
7	2.75	5.5	11	22	44	88	176	352	2.75	5.5	11	22	44
8	1.5	3	6	12	24	48	96	192	3.75	7.5	15	30	60
9													
10	0.75								4.5	9	18	36	72
11	1.75	3.5	7	14	28	56	112	224	1.75	3.5	7	14	28
12													
13													
14													
15													

IV. Operating system

(A) Operating elements

The operating elements and their locations are shown in Fig.2.

(B) Method of operation

1. Main drive system





The speed of the spindle is selected by gear shift lever 8 and 10. Matching the eight gear positions of lever 8 with the three gear positions (except the "white point" position) of lever 10 according to the same color, 24 steps of forward and reverse rotary speeds can be achieved. (as shown in Table I).

When lever 10 is in "white point" position, the spindle being disengaged from the gears of the drive shaft, both revolution of spindle and mechanical feeding are stopped. In this position, if the amplified pitch transmission is engaged, a feeding without spindle revolution can be carried out.

2. Feeding system


a. Selection of thread-pitch or feedrate is effected by actuating lever 5 on the headstock, levers 6, 7 and 9 on the feed gearbox.

1) Normal-and amplified pitches, forward and reverse feed lever 5 is used to change the pitch and the direction of thread or change the feedrate. Since the apron is adapting an overrunning clutch for transmission, so the carriage can be fed only when it is in "right-hand" position.

-  — shows right-hand normal pitches or basic feedrates
-  — shows left-hand normal pitches(no feed)
-  — shows right-hand amplified pitches or reduced or amplified feedrates
-  — shows left-hand amplified pitches(no feed)

2) The major function of thread-type change lever 6 is to select the required type of thread, and certainly can be used to change the feedrates as well.

- t -- shows metric threads
- n -- shows inch threads
- m -- shows module threads
- DP-- shows diametral pitch threads

 --"Direct-Connecting" position, shows the transmission is not passing through the change gears in feed gear-box.

3) The basic gear-ratio change lever 7, being actuated following the sequence from No.1 to No.15 on the circular index plate, can change the threadpitch or feedrates from small to big.

4) The multiplying gear change lever 9 is used to connect the leadscrew or the feeding rod, and multiply the threadpitch or the feedrates.

产品型号	文件代号	第 12
	SY-AB-7	共 61 页
日期		

A, B, C, D; used to connect the lead shaft to the lead gears. Their multiplying ratios are 1:1:1:1:1:1. By setting the above levers, various threadpitches and feedrates can be acquired as shown in Table 2.

The revolving motion of leadscrew may be transmitted not via the variable gear trains in feedbox but driven directly by the transposing gears between output shaft of headstock and input shaft of feedbox to enable the operator to cut threads of special pitch. For this purpose, the thread variety dial knob 6 has to be put on position and the multiplying gear lever 9 on position IV.

b. Operator's control of carriage movement

- 1) The four-way power-feed lever 20 with rapid-travel pushbutton controls the longitudinal and transversal automatic feed and rapid movement of carriage. The hand-pushing direction of lever is just consistent with the required feeding direction of turning tool. When rapid travel is desired, push the lever 20 to the moving direction and press the pushbutton (on the head of the lever) with thumb simultaneously until the required position is reached and then release it.
- 2) For thread cutting, the longitudinal travel of tool is controlled by split-nut closing and releasing lever 17. Turn the lever clockwise for closing and counterclockwise for releasing.
- 3) Manual operation of carriage is carried out by actuating saddle longitudinal travel handwheel 12, cross slide traverse ball crank handle 13 and top slide travel lever 21 according to the scale of their index dials.

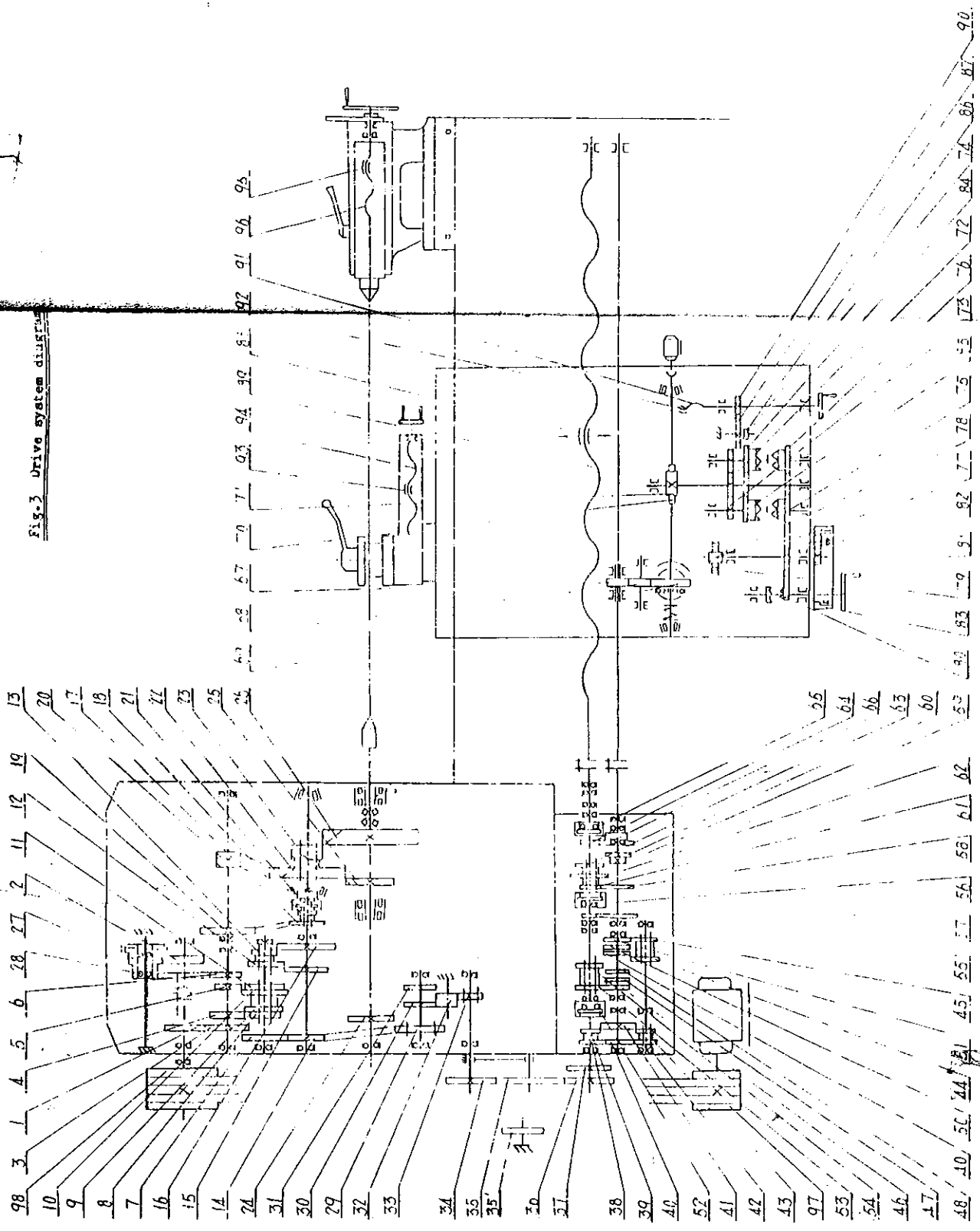
c. The function of other control elements are clarified by their nomenclatures. They are operated following the usual method.

Among them, by lifting the forward-brake-reversing lever 11 or 19 up the main spindle is in forward rotation; by setting it down the main spindle is in reverse rotation, and by setting it in middle position the main spindle will then stop.

Besides, the square turret features that in any case it can be clamped quickly by turning the clamping handle 14 back less than a complete revolution after it has been released for swivelling to displace the tools.

编	产品型号	第 13 页
制	文件代号	共 61 页
	SY-AB-7	
	日期	

Fig-3 Drive system diagram



产品型号	SY-AB-t	第 15
文件代号		共 61
编 号		日期

V. Drive system

(A) Drive system diagram and chief components

The drive system diagram of CY6140B, CY6240B, CY6150B and CY6250B is shown in Fig.3 and the chief components are shown in Table 3.

(B) Kinematic chain of drive system

1. The kinematic chain of main drive

According to the kinematic chain of main drive shown in drive system diagram, the main spindle speeds in revolutions per minute are derived as follows;

$$n_{\text{motor}} \times \frac{D}{178} \times 0.99 \times \frac{45}{40} \times \left\{ \begin{array}{l} \frac{28}{44} \\ \frac{32}{40} \\ \frac{36}{36} \\ \frac{40}{32} \end{array} \right\} \times \left\{ \begin{array}{l} \frac{20}{61} \\ \frac{36}{45} \end{array} \right\} \times \left\{ \begin{array}{l} \frac{30}{48} \times \frac{16}{60} \times \frac{20}{80} \\ 1 \times \frac{20}{80} \\ 1 \times \frac{60}{40} \end{array} \right. \begin{array}{l} \text{8 steps of low-speeds} \\ \text{8 steps of intermediate-speeds} \\ \text{8 steps of high-speeds} \end{array}$$

where n_{motor} -- speed in rpm of main drive motor

D_1 -- pitch diameter of V-belt sheave on motor

$D_1 = 115$ mm for AC Frequency $f = 50$ Hz

$D_1 = 96$ mm for AC Frequency $f = 60$ Hz

0.99 -- Efficiency of belting

The 24 steps of main spindle speeds are thus computed from above formula and listed in Table 1.

2. The kinematic chain of feeding and threading

(1) According to the drive system diagram, the threadpitch of workpiece t_w relating to the feeding gear ratios is as follows:

$$t_w = 1 \times i_h \times i_t \times i_b \times i_m \times T$$

where t_w -- the threadpitch of workpiece to be cut (mm)

i_h -- the mesh ratio of feeding gear train in headstock which is selected by means of lever 5.

for primary feeding: $\frac{48}{48} \times \frac{31}{31} = 1$

for amplified feeding: $\frac{80}{20} \times \frac{60}{16} \times \frac{48}{30} \times \frac{32}{18} \times \frac{48}{48} \times \frac{31}{31} = 16$

for reduced feeding: $\frac{40}{60} \times \frac{32}{48} \times \frac{48}{48} \times \frac{31}{31} = \frac{4}{9}$

文件代号	产品型号
SY-AB-t	
共 41 页	第 16 页

i_t -- the mesh ratio of transposing gears

for constant use:

$$\frac{60}{69 \cancel{87}} \times \frac{57 \cancel{87}}{58} = \frac{15}{14}$$

for inch thread 19 tpi:

$$\frac{60}{69 \cancel{87}} \times \frac{60 \cancel{87}}{57} = \frac{20}{19}$$

for inch thread 11½ tpi:

$$\frac{60}{56 \cancel{87}} \times \frac{56 \cancel{87}}{69} = \frac{20}{23}$$

i_g -- the mesh ratio of thread-type change gears in feed gearbox which is selected by means of dial knob 6.

for metric threads:

$$\frac{28}{27} \times \frac{27}{30} = \frac{14}{15}$$

for inch threads:

$$\frac{30}{41} \times \frac{27}{30} = \frac{27}{41}$$

for module threads:

$$\frac{28}{27} \times \frac{41}{29}$$

for diametral pitch threads:

$$\frac{30}{41} \times \frac{41}{29} = \frac{30}{29}$$

i_b -- the mesh ratio of primary change gears in feed gearbox which is selected by means of lever 7. 15 lever-positions in total.

for metric and module threads

$$\frac{28}{36} \times \frac{18}{21} = \frac{2}{3} \quad (\text{lever-position No. 1})$$

$$\frac{28}{32} \times \frac{18}{21} = \frac{3}{4} \quad (\text{lever-position No. 2})$$

$$\frac{28}{32} \times \frac{20}{21} = \frac{5}{6} \quad (\text{lever-position No. 4})$$

$$\frac{28}{36} \times \frac{33}{28} = \frac{11}{12} \quad (\text{lever-position No. 7})$$

$$\frac{28}{32} \times \frac{32}{28} = 1 \quad (\text{lever-position No. 8})$$

$$\frac{28}{32} \times \frac{36}{28} = \frac{9}{8} \quad (\text{lever-position No. 10})$$

$$\frac{21}{18} \times \frac{21}{21} = \frac{7}{6} \quad (\text{lever-position No. 11})$$

for inch threads and D P threads

$$\frac{21}{18} \times \frac{36}{28} = \frac{3}{2} \quad (\text{lever-position No. 15})$$

$$\frac{21}{18} \times \frac{32}{28} = \frac{4}{3} \quad (\text{lever-position No. 14})$$

$$\frac{21}{21} \times \frac{36}{28} = \frac{9}{7} \quad (\text{lever-position No. 13})$$

$$\frac{21}{20} \times \frac{32}{28} = \frac{6}{5} \quad (\text{lever-position No. 12})$$

$$\frac{28}{32} \times \frac{36}{28} = \frac{9}{8} \quad (\text{lever-position No. 10})$$

产品型号	SY-AD-R
文件代号	
共 61 页	第 17 页

$$\frac{28}{32} \times \frac{22}{28} = \frac{11}{16} \quad (\text{lever-position No. 1})$$

$$\frac{28}{32} \times \frac{32}{28} = 1 \quad (\text{lever-position No. 8})$$

$$\frac{28}{36} \times \frac{32}{28} = \frac{8}{9} \quad (\text{lever-position No. 6})$$

$$\frac{21}{21} \times \frac{18}{21} = \frac{6}{7} \quad (\text{lever-position No. 5})$$

$$\frac{28}{32} \times \frac{18}{21} = \frac{3}{4} \quad (\text{lever-position No. 2})$$

the gear combination $\frac{28}{36} \times \frac{21}{21} = \frac{7}{9}$ (lever-position No. 3) is used for getting feedrates only.

i_m --the mesh ratio of multiplying change gears in feed gearbox which is selected by means of lever 9.

$$\frac{14}{42} \times \frac{15}{40} = \frac{1}{8} \quad (\text{lever-position I or A})$$

$$\frac{14}{42} \times \frac{24}{32} = \frac{1}{4} \quad (\text{lever-position II or B})$$

$$\frac{14}{42} \times \frac{33}{22} = \frac{1}{2} \quad (\text{lever-position III or C})$$

the spur gear couples into the internal gear, $\frac{22}{22} = 1$ (lever-position IV or D)

T--threadpitch of leadscrew (mm). T=12mm

Hence the nominal values of various thread-types are computed in accordance with the following formulas and listed in Table 2.

for metric threads:

$$\text{threadpitch } t = t_w = 1 \times i_h \times i_t \times i_s \times i_b \times i_m \times T \text{ mm}$$

for inch threads:

$$\text{number of teeth per inch } n = \frac{25.4}{t_w} = \frac{25.4}{1 \times i_h \times i_t \times i_s \times i_b \times i_m \times T}$$

for module threads:

$$\text{number of module } m = \frac{t_w}{\pi} = \frac{1 \times i_h \times i_t \times i_s \times i_b \times i_m \times T \text{ mm}}{\pi}$$

for D P threads:

$$\text{number of diametral pitch } DP = \frac{25.4}{t_w} = \frac{25.4}{1 \times i_h \times i_t \times i_s \times i_b \times i_m \times T}$$

The calculating errors of these kinematic chains resulting from above mentioned gear combinations are as follows:

for metric threads $f_t = 0$

for inch threads $f_n = 0.0291/1000$

for module threads $f_m = 0.0540/1000$

for D.P. threads $f_{DP} = 0.0813/1000$

产品型号	
文件代号	SY-AB-7
第 18 页	
共 01 页	

(2) Basing upon the drive system diagram, the feed rates are calculated according to the following formula and substituted into the following formula.

$S_{\text{longitudinal}}$

$S_{\text{transverse}}$

Where $S_{\text{longitudinal}}$ -- the longitudinal feedrates of carriage

$S_{\text{transverse}}$ -- the transverse feedrates of cross slide

i_r -- the mesh ratio of a pair of gears in feed gearbox driving the feed shaft

$$i_r = \frac{21}{42} = \frac{1}{2} \quad i_t = \frac{60}{69 \text{ (or } 87)} \times \frac{69 \text{ (or } 87)}{36}$$

i_{SL} -- the mesh ratio of gear train from feed shaft to bed-rack

$$i_{SL} = \frac{36}{32} \times \frac{32}{56} \times \frac{2}{25} \times \frac{32}{36} \times \frac{45}{87}$$

i_{ST} -- the mesh ratio of gear train from feed shaft to cross slide

$$i_{ST} = \frac{36}{32} \times \frac{32}{56} \times \frac{2}{25} \times \frac{32}{36} \times \frac{45}{40} \times \frac{63}{18}$$

m -- module of spur gear No.79

$m = 2.5 \text{ mm}$

z -- number of teeth of spur gear No.79

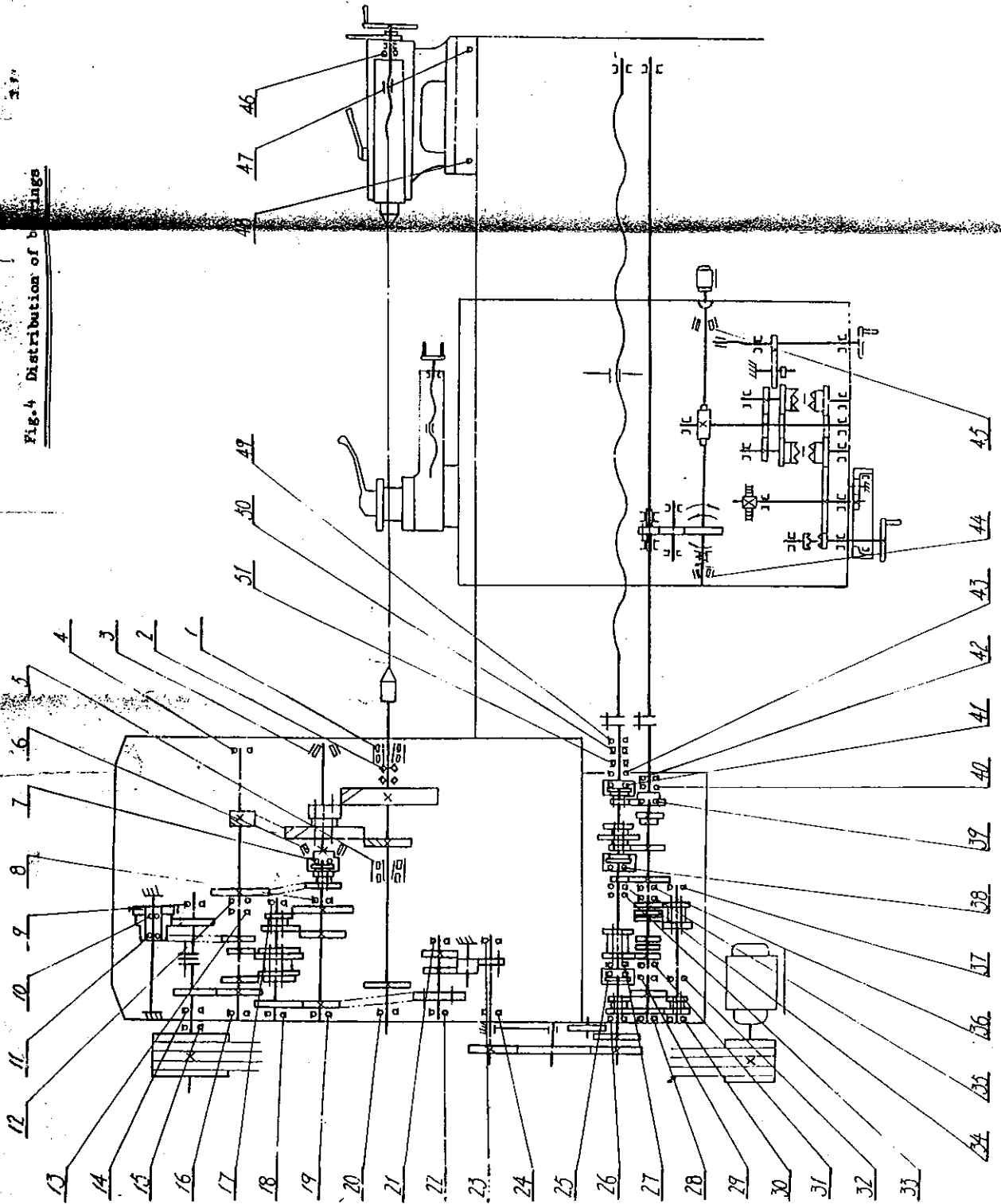
$z = 12$

t_g -- threadpitch of feed screw in cross slide

$t_g = 5 \text{ mm}$

产品型号	
文件代号	57-AB-R
共 19 页	第 61 页

Fig. 4 Distribution of bearings



(C) Distribution and Details of Bearings
 The distribution of ball bearings and their locations in Fig. 4 is shown in Fig. 7, and their details are listed in Table 4.

Table 4 Details of Bearings

No.	Type No.	Specification	Qty	Location No. in Fig. 4
1	7000106	35 x 55 x 9	2	43, 49
2	105	25 x 47 x 12	10	33, 7, 10, 11, 21, 23, 32, 34, 40, 42
3	106	30 x 55 x 13	1	24
4	203	17 x 40 x 12	9	25, 29, 31, 35, 36, 37, 38, 39, 41
5	205	25 x 52 x 15	3	13, 22, 27
6	208	40 x 80 x 18	3	9, 14, 15
7	303	17 x 47 x 14	1	28
8	304	20 x 52 x 15	1	30
9	305	25 x 62 x 17	3	26, 16, 17
10	306	30 x 72 x 19	2	18, 12
11	307	35 x 80 x 21	2	8, 4
12	308	40 x 90 x 23	1	19
13	D119	95 x 145 x 24	1	20
14	D3182120	100 x 150 x 37	1	5
15	1D3182124K	120 x 180 x 46	1	1
16	7205	25 x 52 x 16.5	2	44, 45
17	7209	45 x 85 x 21	1	6
18	7608	40 x 90 x 35.5	1	3
19	D8106	30 x 47 x 11	2	50, 51
20	5D2268124	120 x 180 x 72	1	2
21	8205	25 x 47 x 15	1	46
22	17	7 x 19 x 6	4	47, 48

产品型号
 文件代号 SY-AB-7
 日期
 共 21 页

VI. Electrical system

The principle of electrical system is shown in fig. 6. The electrical system is shown in fig. 6, and the electric equipment is shown in fig. 7. For adapting to the different power systems of various countries, the machine can be provided optionally with electrical equipments of 50 Hz or 60 Hz, in main voltage of 220V, 380V, 420V or 440V and in control voltage of 110V, illuminator voltage of 24V, in motor power of 10HP, 15HP or 20HP.

Before connecting the machine to the mains, it is necessary for our engineers to make sure that the frequency and voltage given on data plate agreed with the local power system. The fuse haven't been provided with the machine and it should be mounted on the power line by the users according to the value of data plate.

The power line should enter the machine through the hole on the left side of the front leg, since the wiring board is also placed to the left of its rear window. An earthing wire is to be led out from side hole and tightened on the screw connecting to the ground. (PE)

While the main switch (QS) is in closing state, the local illuminator (EL1) and the pilot lamps (HL1 and HL2) mounted in green pushbutton (SB2 and SB3) of the main motor will light up, it shows that circuit is being connector to network.

By pressing down the start-pushbutton, the pilot lamp will go out, it shows the command given by pressing green pushbutton is completed and the main motor is being started. Conversely, if press the red pushbutton (SB4), the the main motor will be stopped.

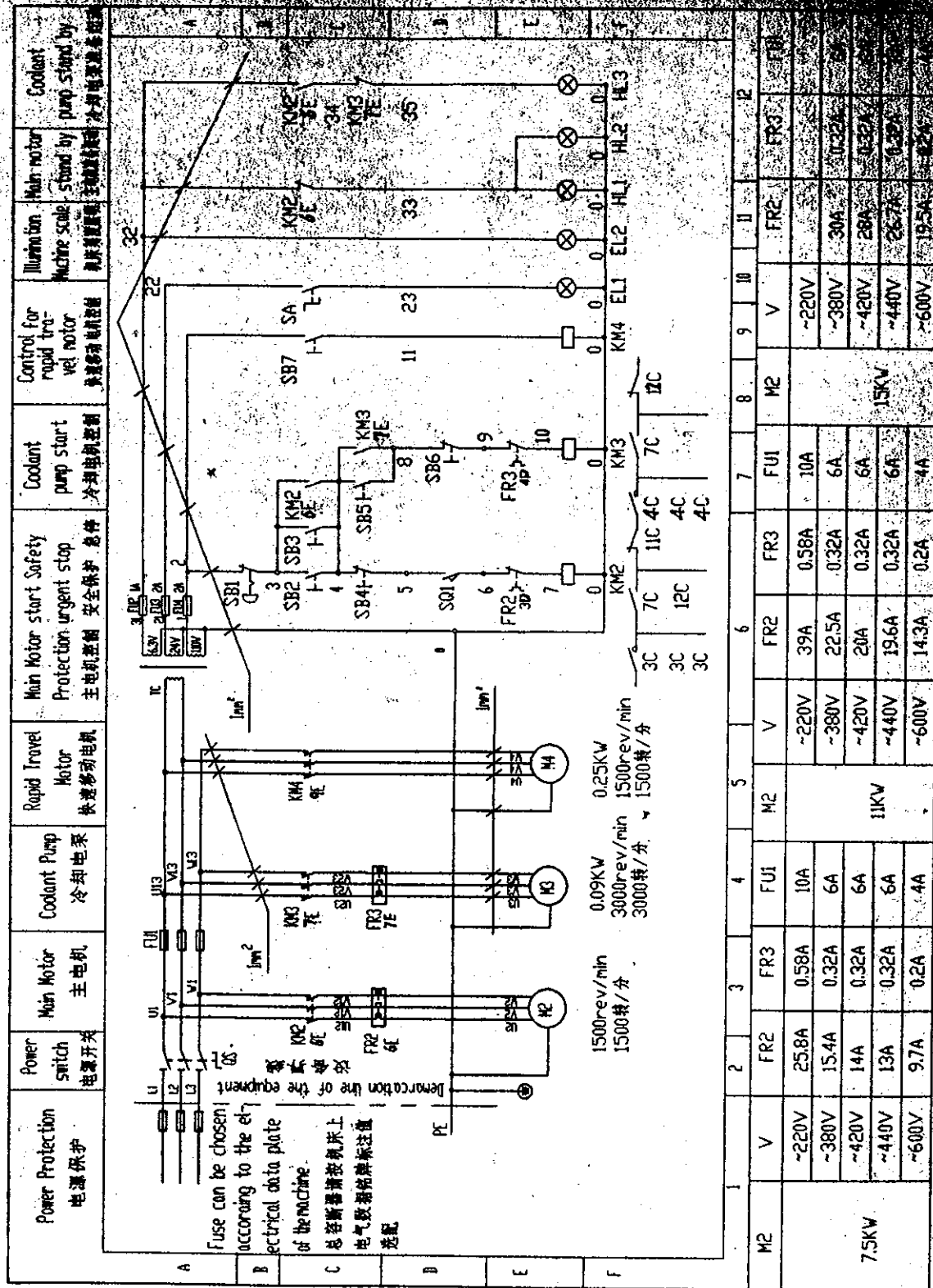
After starting the main motor, the pilot lamp (HL3) mounted in green pushbutton (SB5) of the coolant pump (M3) will light up and by pressing this pushbutton, the coolant pump will be started, the pump will be stopped automatically or restarted following the switching-off-or-on of the main motor.

A safety switch (SQ) is built in the belt cover, the main motor can't be started when opening the cover. An urgent stop-pushbutton (SB1) on the pushbutton plate can cut off all the circuits and beep the machine out of running when occurring some unexpected accident. After removing the obstacle, make sure to turn the urgent stop-pushbutton in direction of an arrow to 30° restoration, then the machine can be restarted.

After connecting all the circuits, illuminating can be controlled by the switch mounted on the pilot lamps (EL1); the rapid travel motor of slide can be controlled also by the black rapid travel pushbutton (SB7).

A hanger hole for the naked lock is also provided with the power switch of the machine. Various naked locks can be equipped at the customers choice. Special tools for opening the electrical equipment cabinet are available in accessory box.

产品型号	
文件代号	SY-AB-7
编制日期	
共	第
页	页

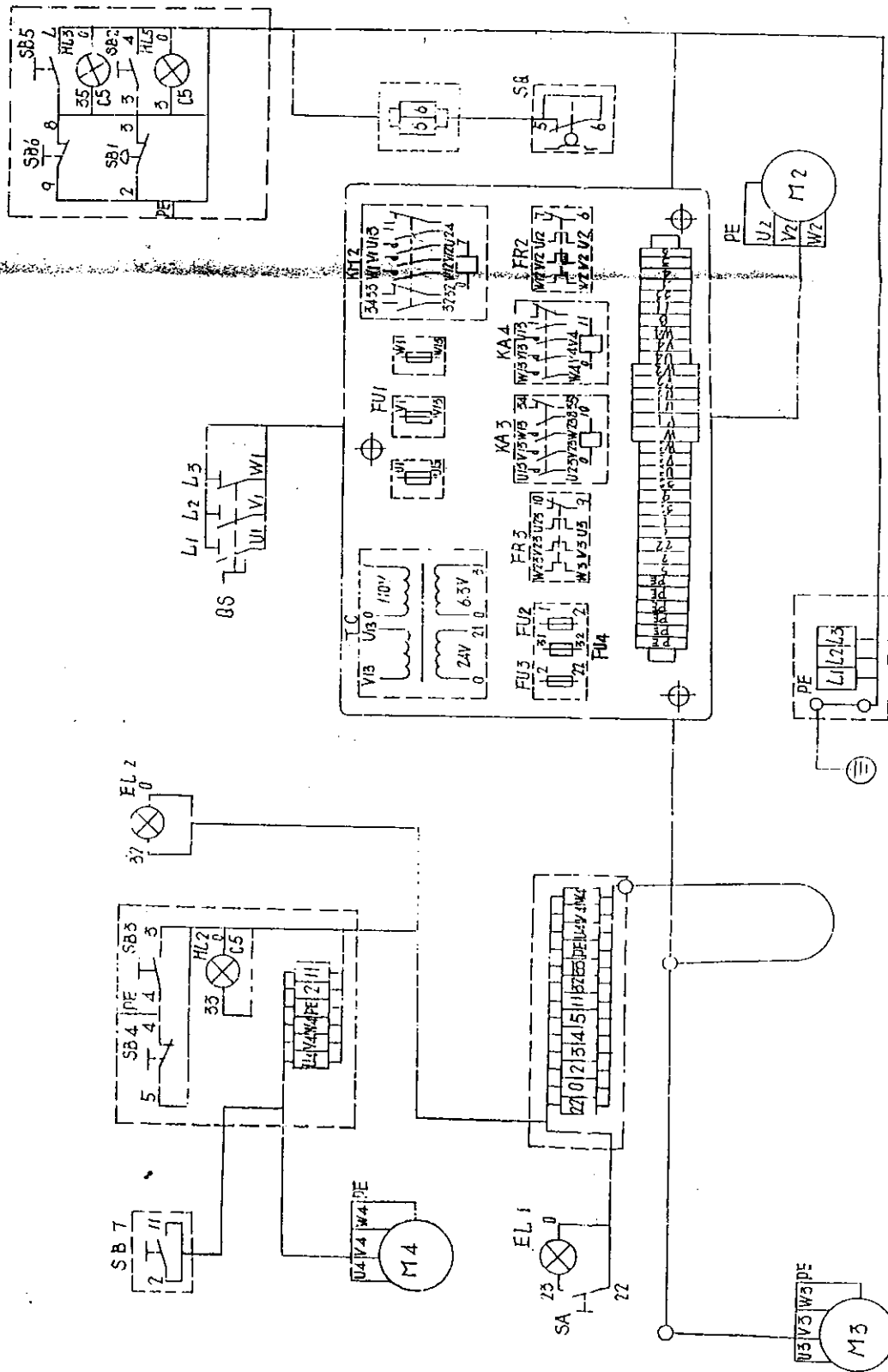


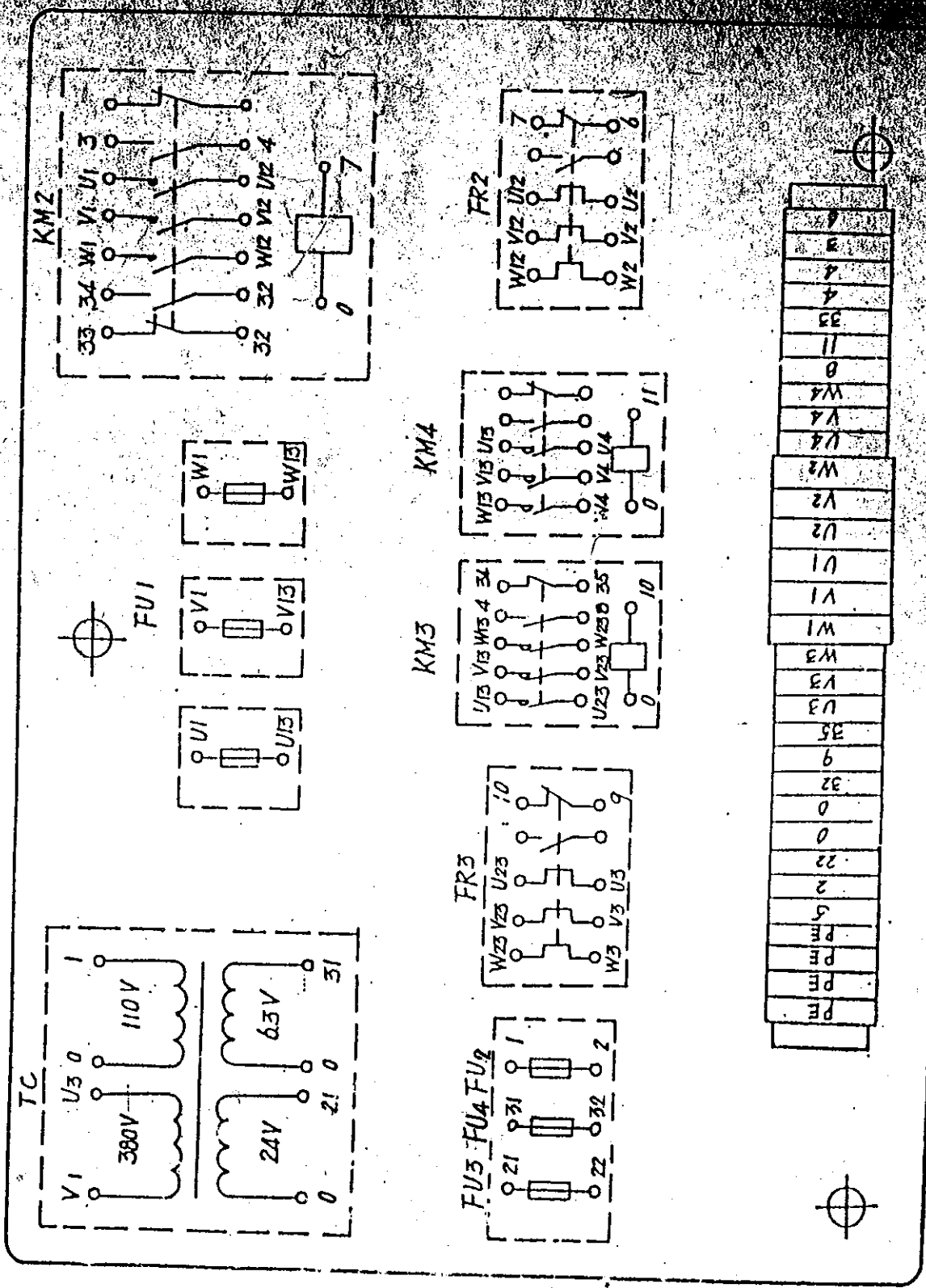
Note: the value of thermal relay is the reference value, using the marked value on the data plate as standard. Users must take care of this.

注：各过热继电器整定值为参考值，以各电机铭牌标注值为标准，请用户注意。

The principle of electrical equipments
电气原理图

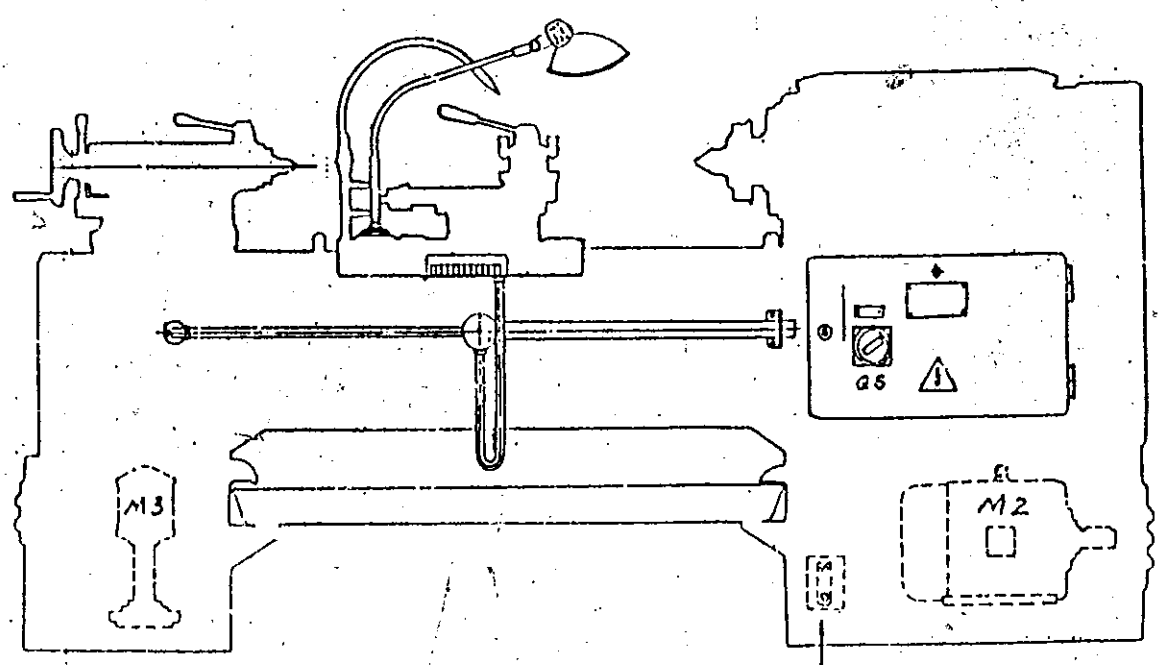
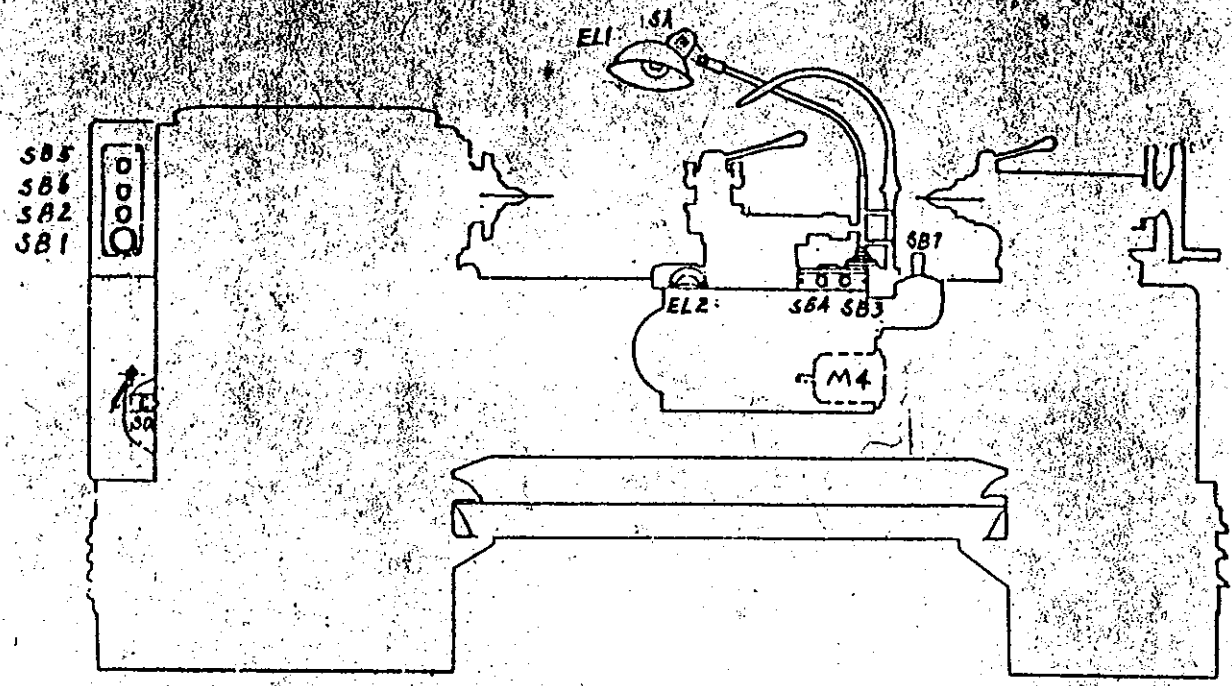
Fig.6 Electrical wiring diagram





Location diagram

Wiring Diagram



Power 3 ~ 50Hz PE
50A Fuse 4X4 mm² cu

产品型号	CY614Q	第	页
文件代号	SY-AB-7	共	页
日期			

Table 6. List of electric equipments

No. of electric equipments	No. of electric diagrams	Names and applications	Technical parameter	Quantity	Reference Model
SB1	7	Pushbutton. Emergency stop Selflocking Mushroom	$U_e: 380V \sim$, $I_{th}=5A$ $\phi 35$, red 1 (b).	1	LA19-D1JZ
SB2	7	Main motor start	$\phi 28$ green, 1 (a) + 1 (b)	1	LA19-11D
SB3	8	"	lamp, 6.3V, 1W, BA9S	1	LA19-11D
SB4	7	Main motor stop	$\phi 28$ red, 1 (a) + 1 (b)	1	LA19-11
SB5	8	Cooling pump start	$\phi 20$ green, 1 (a) + 1 (b) lamp, 6.3V, 1W, BA9S	1	LA19-11D
SB6	9	Cooling pump stop	$\phi 20$ red, 1 (a) + 1 (b)	1	LA11-11
SB7	10	Rapid travel motor start	$U_e, 300V \sim$, $I_{th}=2.5A$ black, 1 (a) + 1 (b)	1	LA9
SQ	7	Limit switch	$U_e, 380V \sim$, $I_{th}=5A$ 1 (a) + 1 (b)	1	LX19K
EL1	11	Work lamp	24V \sim , 40W lamp holder E27	1	JC11-1
EL2	12	Pilot lamp	6.3V \sim , 1W, colorless, BA9S	1	XD-0
FU1	3	Fuse	fuse link: 6A used for power of $\begin{cases} 600V \\ 380V \\ 420V \\ 440V \end{cases}$ 10A used for power of 220V	3	QM3
FU2	7	Fuse	fuse link: 1A	1	} 9F1
FU3	7	Fuse	fuse link: 2A	1	
FU4	7	Fuse	fuse link: 2A	1	
TC	6	Control transformer	primary: $\begin{cases} 220V \\ 380V \\ 420V \\ 440V \end{cases}$ 50HZ (60HZ) secondary: 110V, 100VA (85VA) 24V, 45VA (70VA) 6.3V, 5VA (5VA)	1	depending on the power voltage of the principle of electrical diagram reference model (JBK-160)

Continue

No. of electric equipments	No. of electric diagram	Names and applications	Technical parameter	Quantity	Remarks (Reference model)
QS	2	Power switch	threephase Ue, 500V ~ Ie, 25 A	1	HY1-25-SG used for: power 420V ~ 440V ~ 600V ~ main motor: 7.5Kw
			threephase Ue, 380V ~ Ie, 40 A		HY1-40-SG used for power: 220V ~ main motor: 7.5Kw power: 220V ~ 380V ~ main motor: 11Kw
			threephase Ue, 380V ~ Ie, 25 A		HY1-25-SG used for: power: 380V ~ main motor: 7.5Kw
M 2	3	Three phase squirrel-cage motor Leg mounting type	7.5KW, 1500r.p.m insulation in E class 50HZ (60HZ)	1	Y132M-4 corresponding power: 220V ~ 380V ~ 420V ~ 440V ~ 600V ~
			7.5KW, 1500r.p.m insulation in E class 50HZ (60HZ)		Y160M-4 corresponding power: 220V ~ 420V ~ 440V ~ 600V ~

No. of electric equipments	No. of drawings	Name and application	Technical parameters	Quantity	Reference (model)
M 4	4	Three phase motor pump	0.07Kw, 3000r.p.m insulation in E class 50HZ (60HZ)	1	30B 25 corresponding power: 220V~ 380V~ 420V~ 440V~ 600V~
M 4	5	Three phase squirrel-cage motor Flange mounting type	0.25Kw, 1500r.p.m insulation in E class 50HZ (60HZ)	1	20DS5634 corresponding power: 220V~ 380V~ 420V~ 440V~ 500V~
KM 2	7	Contactor	triple-pole, Ue, 380V~ Ie, 20A/AC3 coil, 110V~, 50HZ (60HZ) auxiliary contact head Ue: 110V~, Ith=5A 2 (a) + 2 (b)	1	3TB4317 suitable for power: 380V~ main motor: 7.5Kw
			triple-pole, Ue, 380V~ Ie, 40A/AC3 coil, 110V~, 50HZ (60HZ) auxiliary contact head Ue, 110V~, Ith=5A 2 (a) + (b)		3TB4417 suitable for power: 220V~ 380V~ main motor: 11Kw power: 220V~ main motor: 7.5Kw
			triple-pole: Ue, 550V~ Ie, 20A/AC3 coil, 110V, 50HZ (60HZ) auxiliary contact head Ue, 110V~, Ith=5A 2 (a) + (b)		3TB4317 suitable for power: 420V~ 440V~ main motor: 7.5Kw

No. of electric equipments	No. of electric diagram	Name and applications	Technical parameter	No.	Remarks
KM3 KM4	9 10	Contactor relay	coil, 110V~ 50HZ (60HZ) Ue, 380V~, Ith=5A 4 (a) + 4 (b)	2	suitable for power: 220V~ 380V~
FR 2	3	Overcurrent relay	current range/rated value 11-22A/15.4A 10-16A/14A 10-16A/13A 20-32A/25.8A 20-45A/39A 9~12.5/9.8A 12.5~18/14.5A	1	JRS2-25/F power: 380V~ main motor: 7.5Kw JRS2-25/F power: 420V~ main motor: 7.5Kw JRS2-25/F power: 440V~ main motor: 7.5Kw JRS2-63/F power: 220V~ main motor: 7.5Kw JRS2-63/F power: 220V~ main motor: 11Kw power: 600V~ motor 7.5KW power: 600V~ motor 11KW

Tool Work

Operating

No. of electric equipments	No. of electric circuits	Reason and applications	Technical parameter	
FR 2	1	Overcurrent relay	current range/rated value 20-32A/22.5A	JRS-25/F power: 380V~ main motor: 11kw
			14-22A/20A	JRS-25/F power: 420V~ main motor: 11kw
			14-22A/19.6A	JRS-25/F power: 440V~ main motor: 11kw
FR 3	4	Overcurrent relay	current range/rated value 0.45-0.72A/0.58A	1 JRS-125/F suitable for: power: 220V~ 50Hz
			0.25-0.35A/0.32A	JRS-125/F suitable for: power: 380V~ 420V~ 440V~
			0.15~0.22/0.2	Power, 600V~

VII. Lubricating system

The lubricating system diagram is shown in Fig.7.

This machine is lubricated mainly by adopting No.30 machine oil with viscosity 3.81°--4.59°, E50.

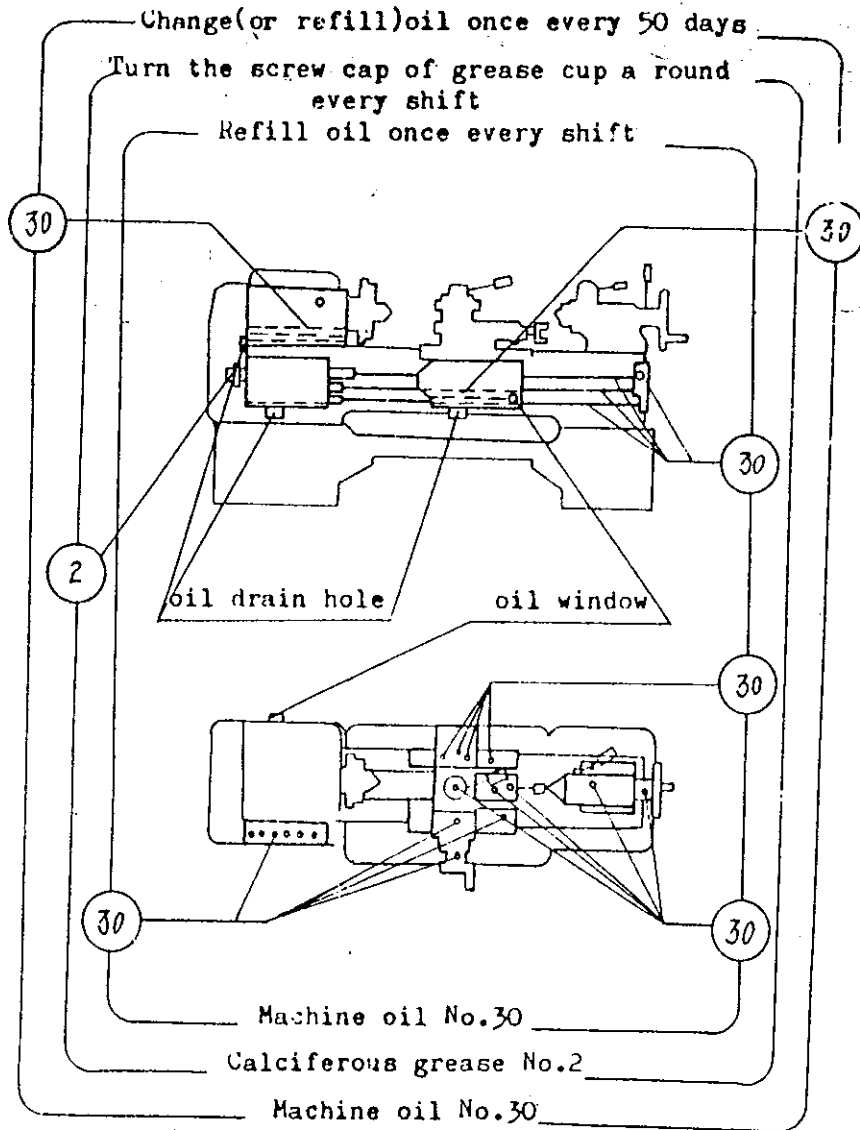


Fig.7 Lubricating system diagram

1. In the headstock the lubricating oil is supplied by a built-in trochoid pump driven by shaft 1 (Fig.8). The lubricant being raised and filtered, is then led to the oil pan and sump for lubricating gears, shafts as well as bearings. A circulatory lubrication is formed in the headstock. (Fig.9). For check up the working condition of the pump, it provides an oil window on the headstock front. The oil level of headstock is observed from the sightglass at the rear side.

编	文件代号	产品型号
制	SY-A8-t	
日		
期		
	共 6 页	第 26 页

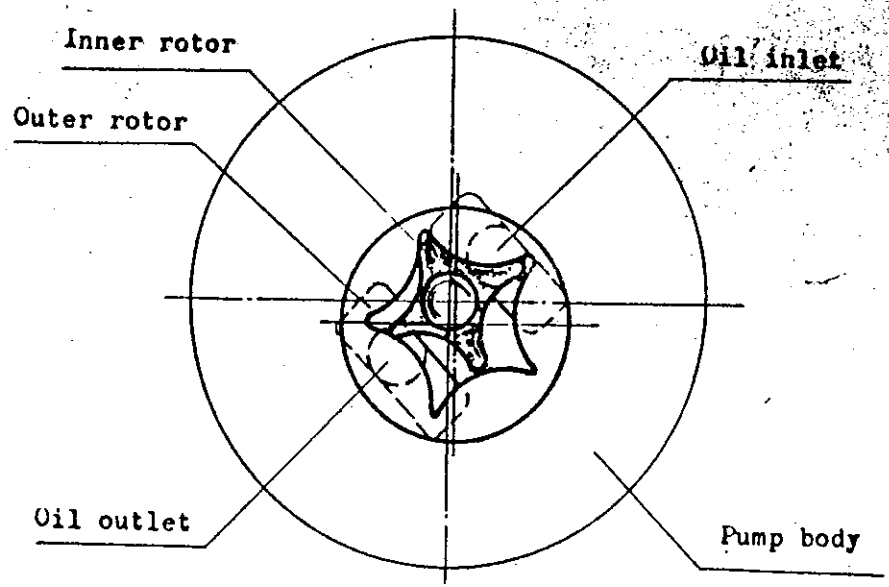


Fig.8 Schematic sketch of trochoid pump in operation

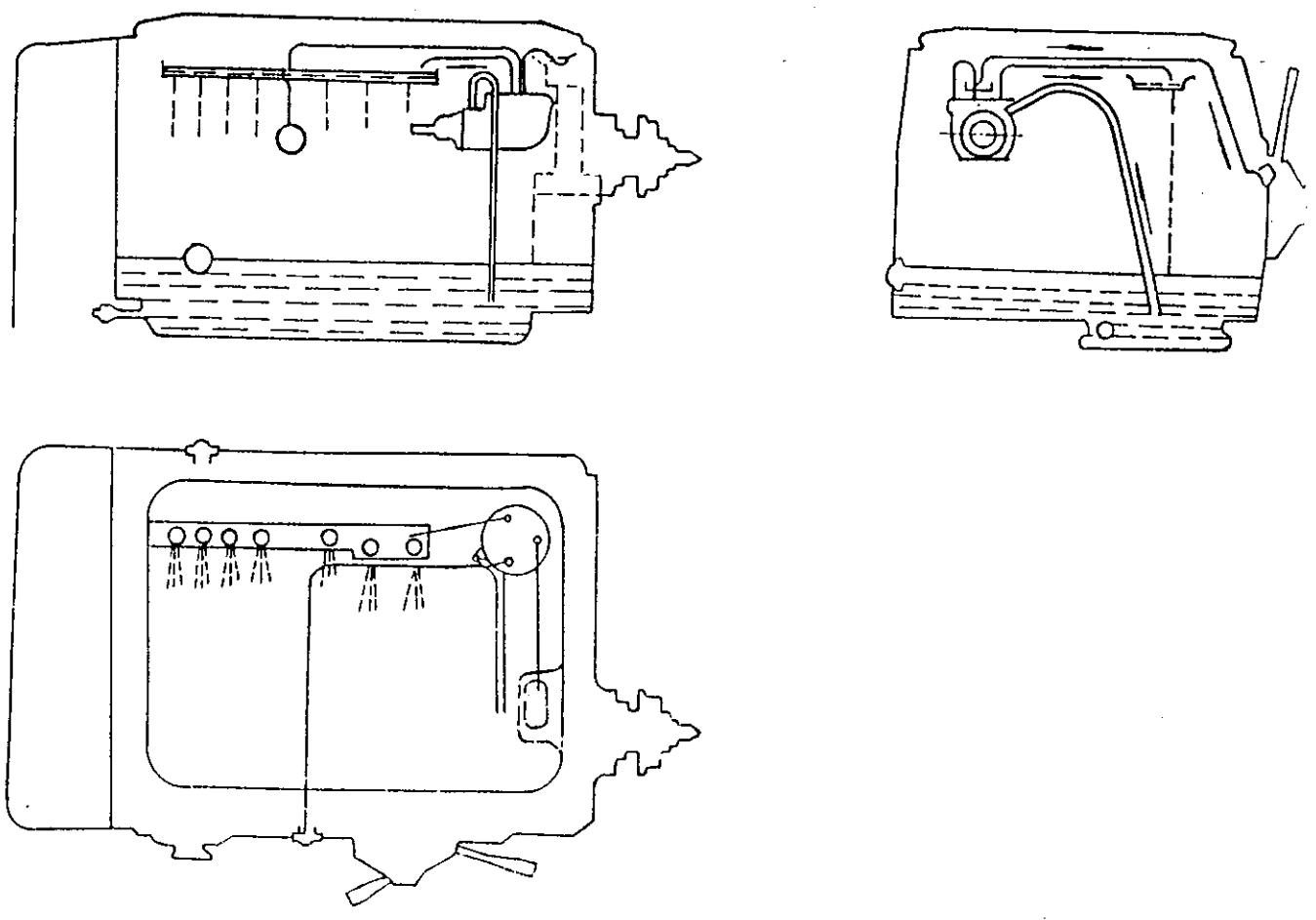


Fig.9 Lubricating diagram in headstock

编	文件代号	产品型号	第 27 页
制	SY-A8-4		共 61 页
日期			

2. The sump on top of feed box is used to reservoir lubricant. The part of the feed box are drop-lubricated through capillary woolen yarns in sump. After a period of operation, drain the waste oil according to the indication on sightglass. (Fig.10).

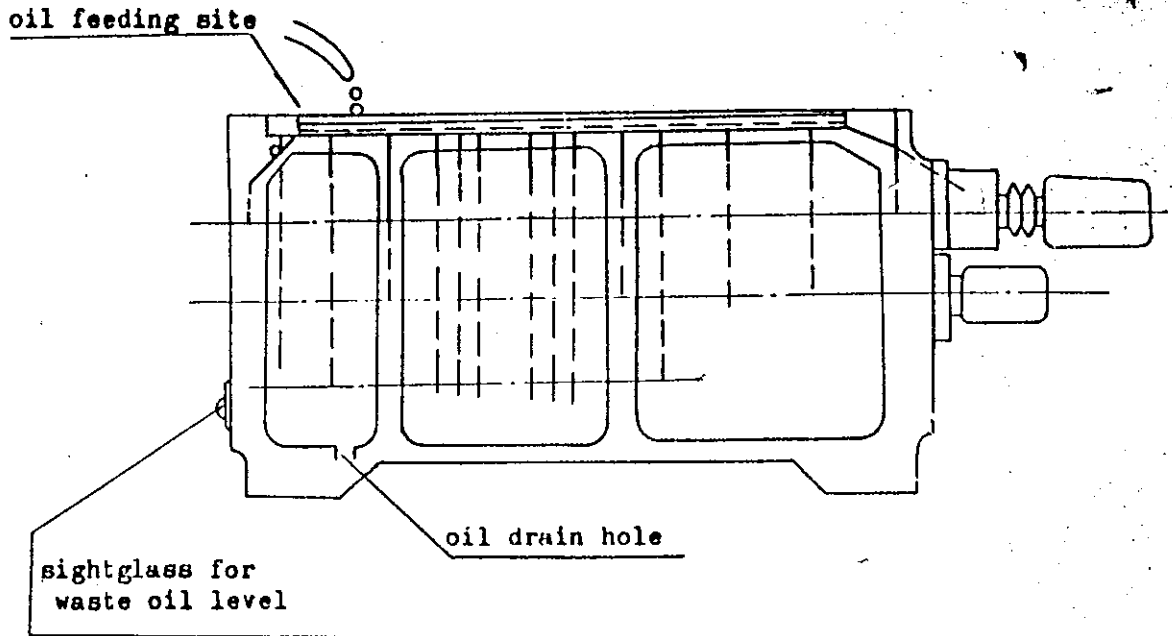


Fig.10 Lubricating diagram in feed gearbox

3. In the apron the internal sump is used to reservoir lubricant, the driving parts are splash-lubricated by the oil agitator during rapid travelling. Bearings in the apron are lubricated either by pressing machine oil through the cup on the saddle with oil gun, or drop-lubricated from the capillary woolen yarns in the top groove which reserve a part of the splashed oil. (Fig.11). The oil lever can be observed in sightglass at the front of the box.
4. The lower guideways of the saddle is lubricated by the through fine felt filtered oil reserved in two cups located in front and in rear each.
5. The upper guideways of the saddle, the transverse feed screw, the leadscrew of the top slide as well as quill and leadscrew of tailstock are all lubricated by oil gun.
6. End journals of the longitudinal leadscrew, feed shaft and reverse shaft are drop-lubricated by capillary woolen yarns in the oil reservoir at the top of the end journal bracket.
7. Idler shafts and sleeves of the transposing gear holder are lubricated with No.2 calciferous grease extruded by means of the screw cap of grease cups.

产品型号	
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共	第 2/2 页

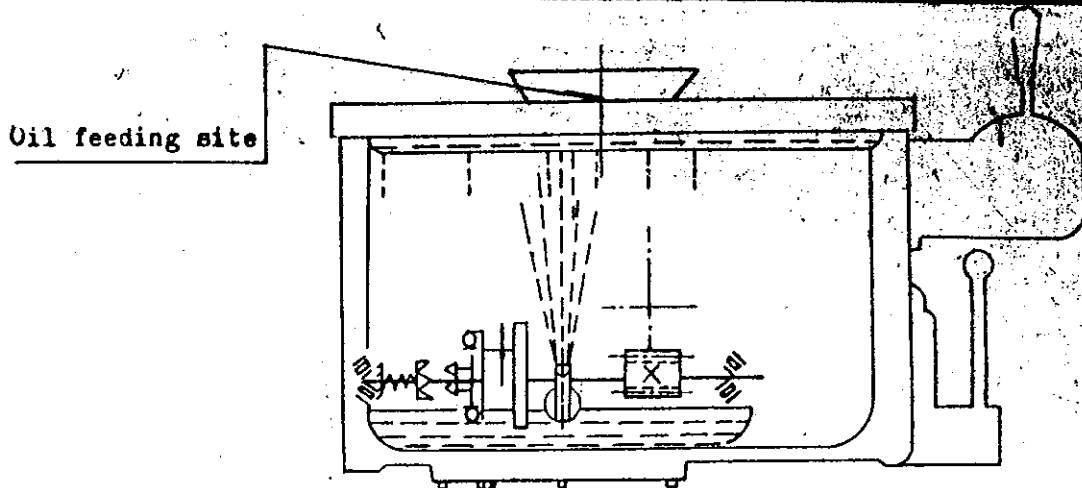


Fig.11 Lubricating diagram in apron

VIII. Cooling system

Coolant of this machine is stored in the rear cabinet leg for machine center distance up to 1500mm or in the middle cabinet leg for machine center distance of 2000mm. The circulation of coolant is effected by an AOB-25 three-phase electric pump. Coolant flow is regulated by a service cock on the coolant pipe.

IX. Construction and adjustment

- 1. Bed: The guideways of bed is induction-hardened.
Main drive motor and coolant pump of the machine are installed in the front and rear (ormiddle) cabinet legs respectively. The power board is located in the square frame at the rear of bed. Tension of the main drive belts should be adjusted appropriately by means of the adjusting nuts. (Fig.12)

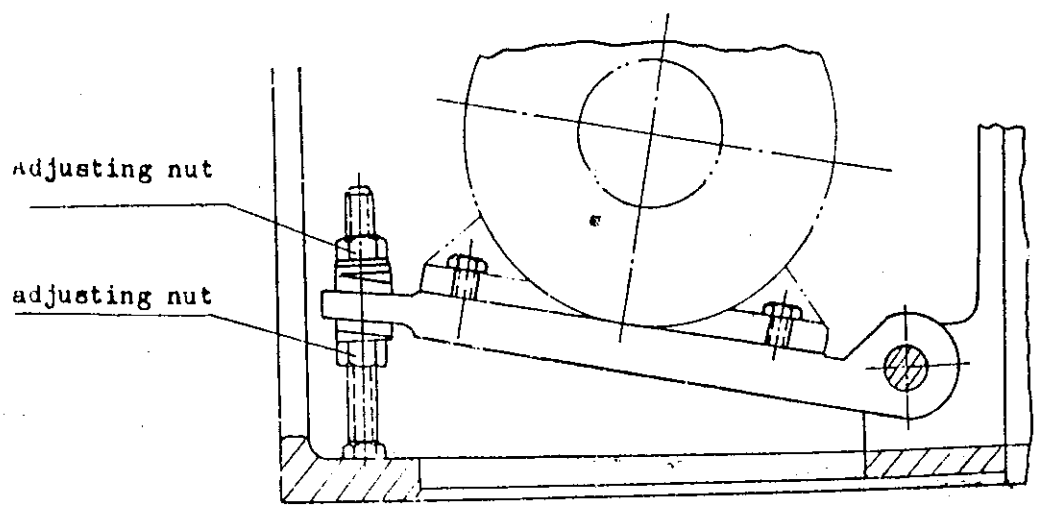


Fig.12 Adjusting diagram of drive belts

编	文件代号	产品型号
制	SY-A8-t	
日期		
		第 21 页
		共 61 页

2. Headstock

This machine adopts centralized all-gear drive system. Shaft 1 is driven by main drive motor through V-belts, and the revolving motion via multi-disc friction clutch and intermediate gears is then transmitted to the main spindle. The revolving direction of the spindle is controlled by the friction clutches. For ensuring a normal working state of main spindle, the friction clutches have to be adjusted appropriately. If it is too loose, starting will not be sensitive and power output of spindle will be reduced, slipping and heat-up may occur frequently, causing serious wear of clutch; if too tight, it will be hard to operate and will lose the effectiveness of safeguard. (Fig.13) After the friction clutches being disengaged, the rotation of the main spindle is then stopped by the brake. When the brakeage can't be realized within a sho time, the adjusting nuts can be used to tighten the brake band appropriately, but pay attention don't let the band be tortured! (Fig.14).

In the headstock, the main spindle adopts a three-point-supporting system, therein take the front and central bearings as chief supporters while the rear bearing as an auxiliary supporter.

In order to assure the machining precision and the cutting performanee, the clearance of spindle bearings should be adjusted carefully making the radial and axial accuracies in rotation of spindle up to the national standards of the machine tools precision. (Fig.16).

When the accuracies do not fulfil above mentioned requirements, proceed an adjustment as follows: Remove stud 8(Fig.16). through the opened hole insert the end of knurled head shaft AB13001 (see Table 7. Service tools) into the blind hole of nut 1. Then loose nut 1 by rotating the main spindle reversely and loose nut 2 after removing the lock-key. Thus nut 3 and nut 4 can be turned to adjust the front bearing and central bearing. After the completion of adjustment, the loosend parts should be tightened and put in place again.

The machine must be tested in an idle-running at max. speed for more than two hours after the adjustment is accomplished. Under a normal running condition of an even rise in temperature, the final temperature of the spindle should not exceed 70°C, if not, the bearings must be readjusted.

The balance weights fixed in the V-groove on gear 5 are set accordingly to eliminate the chattering of spindle during idle-running. The spindle has been balanced and rectified before delivery.

Around the circumference of main spindle flange a graduation of 48 lines has been engraved and an adjustable arrow is set by the side as a scale indicator to facilitate the dividing work in cutting multiple-threads of 9 kinds of starts (i.e. 2, 3, 4, 6, 8, 12, 16, 24, and 48 starts). Before starts-dividing in operation, the spindle speed change lever 10(Fig.2) should be put to "White point position(neutral) at first and jot down the scale of graduation exactly opposing

产品型号	SY-AB-t	第 30 页
文件代号		共 41 页
编 号		
日期		

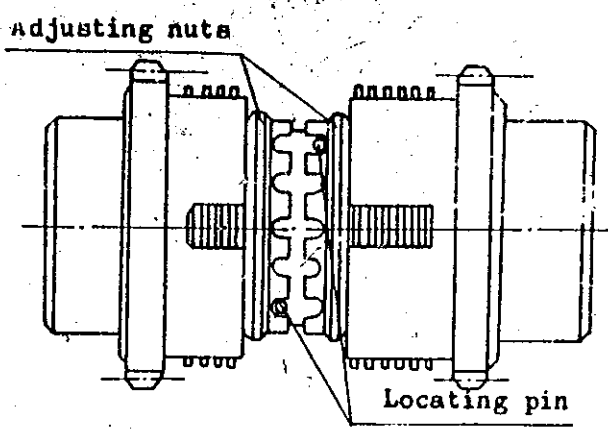


Fig.13 Diagram for adjusting the multi-disc friction clutches

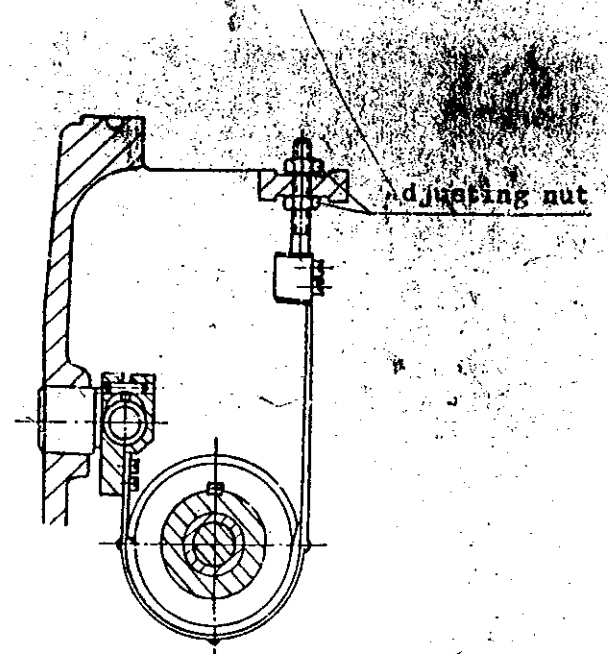


Fig.14 Diagram for adjusting braking band

to the adjustable arrow. After disengaging the normal- and amplified pitches forward and reverse feed lever 5, the spindle can then be turned by hand 48/Z divisions forward or reversely from the indicating scale in accordance with the desired direction. (Z=No. of starts of workpiece). Thereafter engage lever 5 and put lever 10 to original position. The workpiece in operation is now ready for cutting an another start of the multiple-thread.

Chain drive device is employed for shifting the basic gear group in main power transmission. When the chain is slackening, the exactitude of lever position on the circular plate of revolution-numbers would be affected. Under this condition the chain must be tightened by adjusting screw (Fig.15).

3. Tailstock

At the end of quill taper bore a stopper 6 is mounted to prevent the tool's taper shank from rotating. The body of tailstock can be moved transversally on base plate along the single-side guide rail, and its position on base plate is adjusted by screw 1. Loosen the clamping elements

and screw 2 before moving and tighten them after setting. (Fig.17). When replacing the tailstock, right align the convex block on the body with the convex block 8 on base plate.

Being moved longitudinally, the tailstock can be immediately clamped on bed by the eccentric shaft. its clamping force may be regulated by nuts 3 and 4, and when the tailstock is loaded by heavy work,

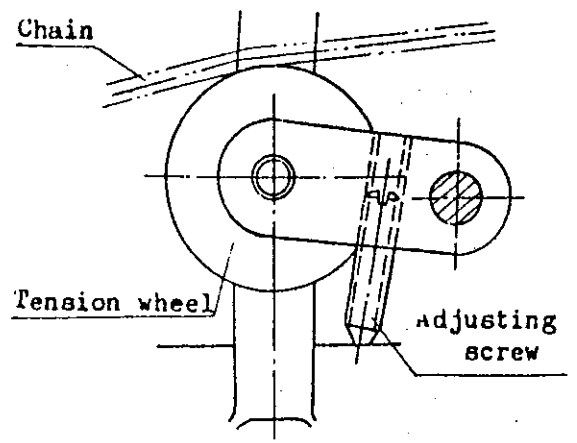


Fig.15 Diagram for adjusting the tension of chain

编 号	产品型号	SY-A8-t	第 31 页
文 件 代 号			共 61 页
日 期			

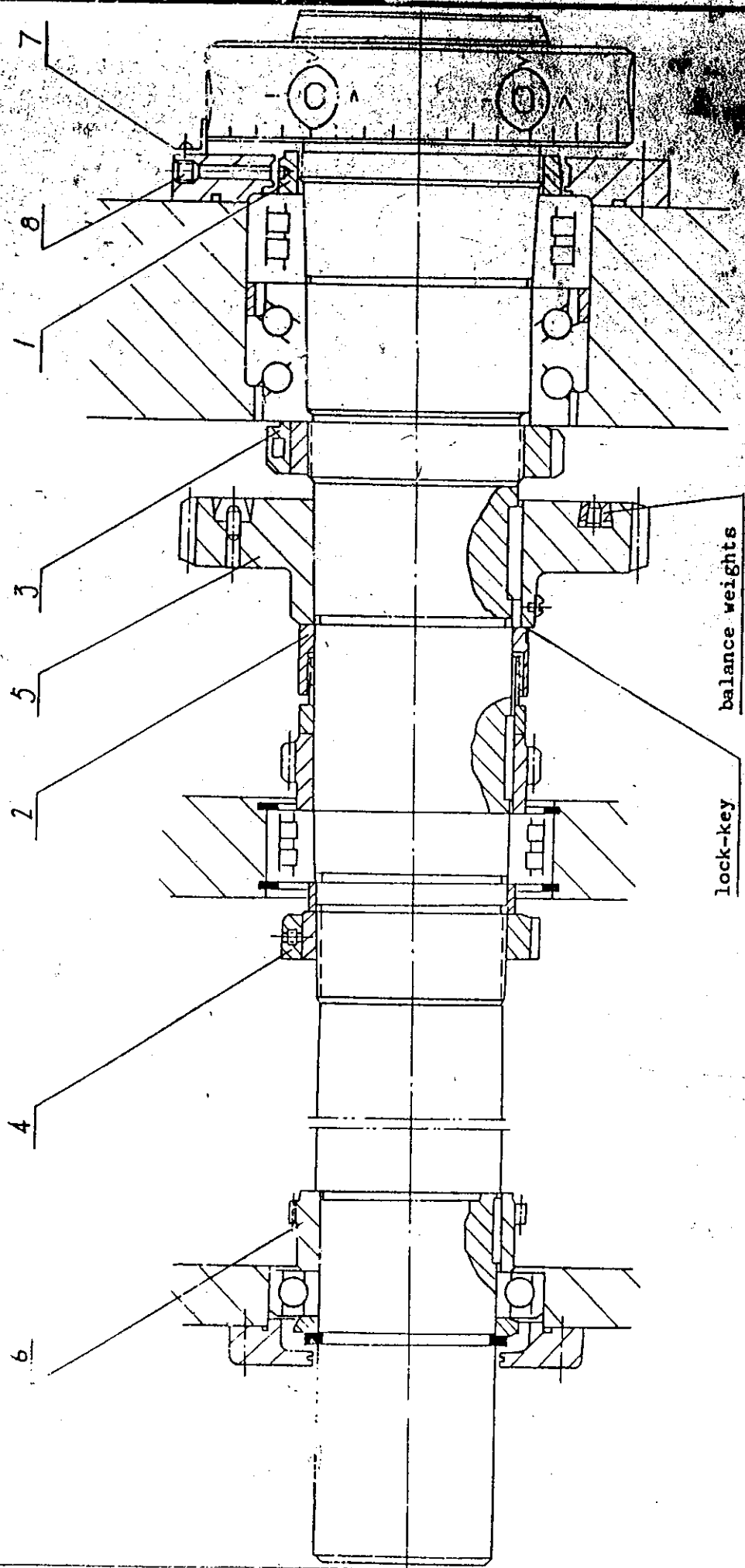


Fig. 16 adjusting diagram of spindle bearings

产品型号	文件代号	日期	共 34 页
	SY-AB-t		
编制			

tighten nut 5 also for ensuring a powerful clamp.
 After loosening the clamping handle, through the underneath four ball bearings with elastic support, the tailstock will be floated about 0.05 -- 0.15 mm on the bed ways to reduce the friction or manual pushing force in moving along the bed-guideways. The floating amount is rather small and adjusted by screw 7. This adjustment can only be made when the tailstock is being clamped on the bed so as to ensure the rigidity of contact between tailstock and bed as well as to prevent the bearings from being crushed.

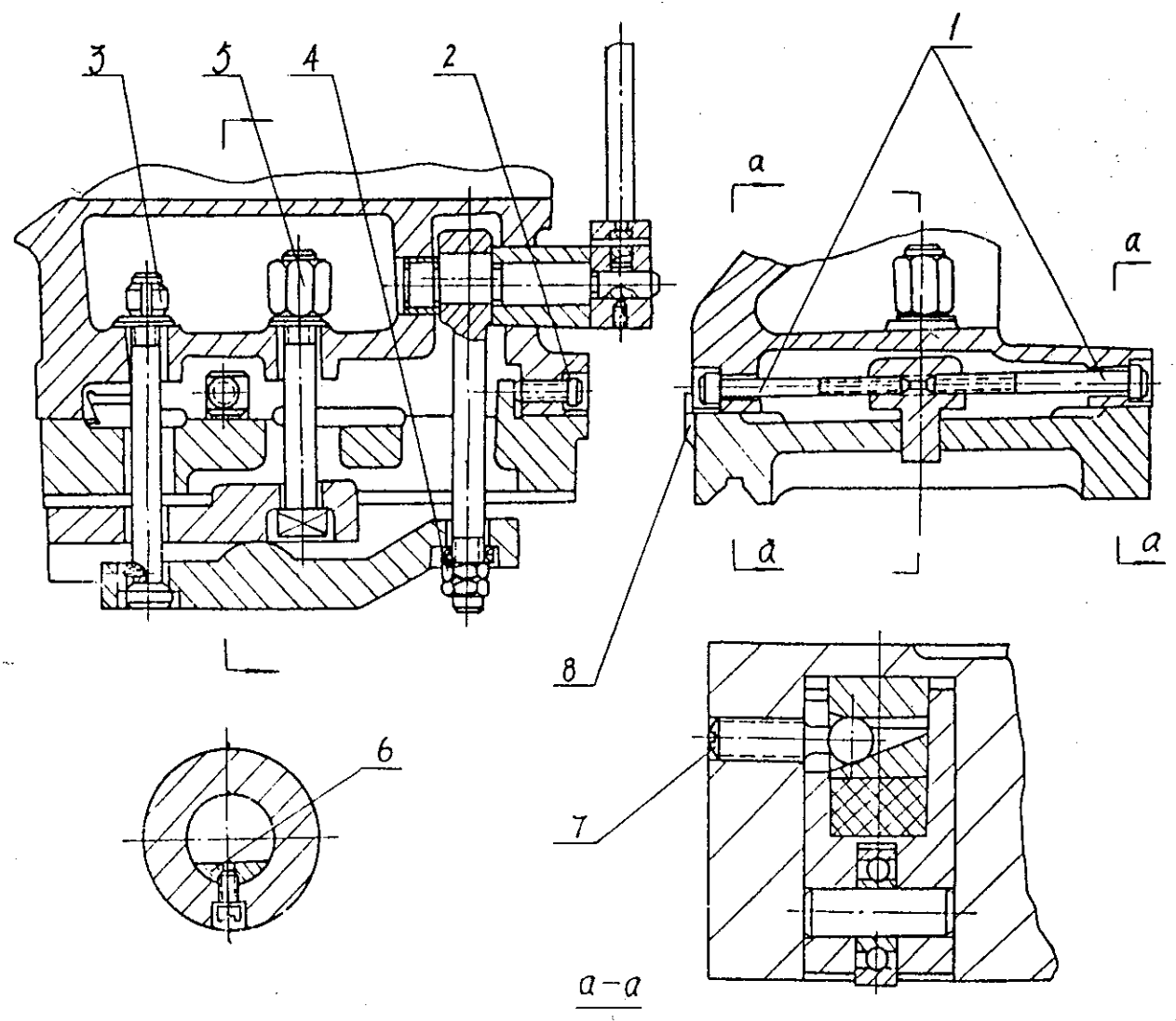


Fig.17 adjusting diagram of tailstock

编	文件代号	产品型号
制	SY-A8-6	
日期		
	共 4 页	第 3 页

4. Carriage

In order to make the square turnable for tool-setting a cam driven by a single-direction pawl is used to lift up a locating pin from the top slide (Fig.18). When rotate the clamping handle counterclockwisely the square turret will be slightly lifted and the lift-up remains constant in many a time and oft operations. In all cases, following every tool setting the square turret can be clamped tightly by rotating the handle clockwise less than a complete revolution.

If the square turret can't be shifted to the proper position during tool-setting try to loosen the spring 5, and conversely, if overstepped, try to tighten it. But this adjustment would not be too tight, otherwise the pressure of spring 5 on ball should exceed the pressure of spring 6 on locating pin, it would not only make the tool-setting strenuous, but also influence the locating accuracy of square turret.

The clamping handle and square turret can be detached for cleaning, having first removed the bolts 1 and 2 as well as the spring 3. The square turret should be reassembled according to the sectional views shown in Fig.18.

The movement of cross slide is effected through a nut driven by the feed screw. This screw nut is of a slotted integral type so as to facilitate the adjustment of a right fit on pitch diameter and to eliminate the driving clearance. When adjusting, loosen stop screw 1 first and then set screw 2 until clearance is removed, thereafter retighten stop screw 1 and put dust cap 3 on (Fig.19).

If the play of the cross slide guideway or of the top slide guideway is too big, or the movement is not sensitive, the adjusting screws in noses at both ends of the gibs can be used for regulating.

Position locking devices are provided for top slide, cross slide and saddle respectively. If any of these parts requires position fixing on guideways, it needs only to tight up the relevant lock screw.(see Fig.2 Lock screw of saddle 16 and Fig.20).

5. Apron

The transversal or longitudinal travel of carriage is realized through the feeding mechanism of the machine. The feeding movement is transmitted into apron by feed shaft, passing through the overload clutch and wormgearing to the driving gear etc.

An one-way overrun clutch is mounted on the worm shaft to enable rapid travelling of the carriage at any time, that is, when the worm shaft is driven in a definite direction by the rapid travel motor, the feeding movement from the feed shaft will be run over.

For safety in operation, the longitudinal travel handwheel will disengage automatically when the carriage is in longitudinal power feeding or rapid travelling. It will engage again automatically as the above mentioned movement

编	文件代号	产品型号
制	SY-AB-7	
日期		
	共 4 页	第 24 页

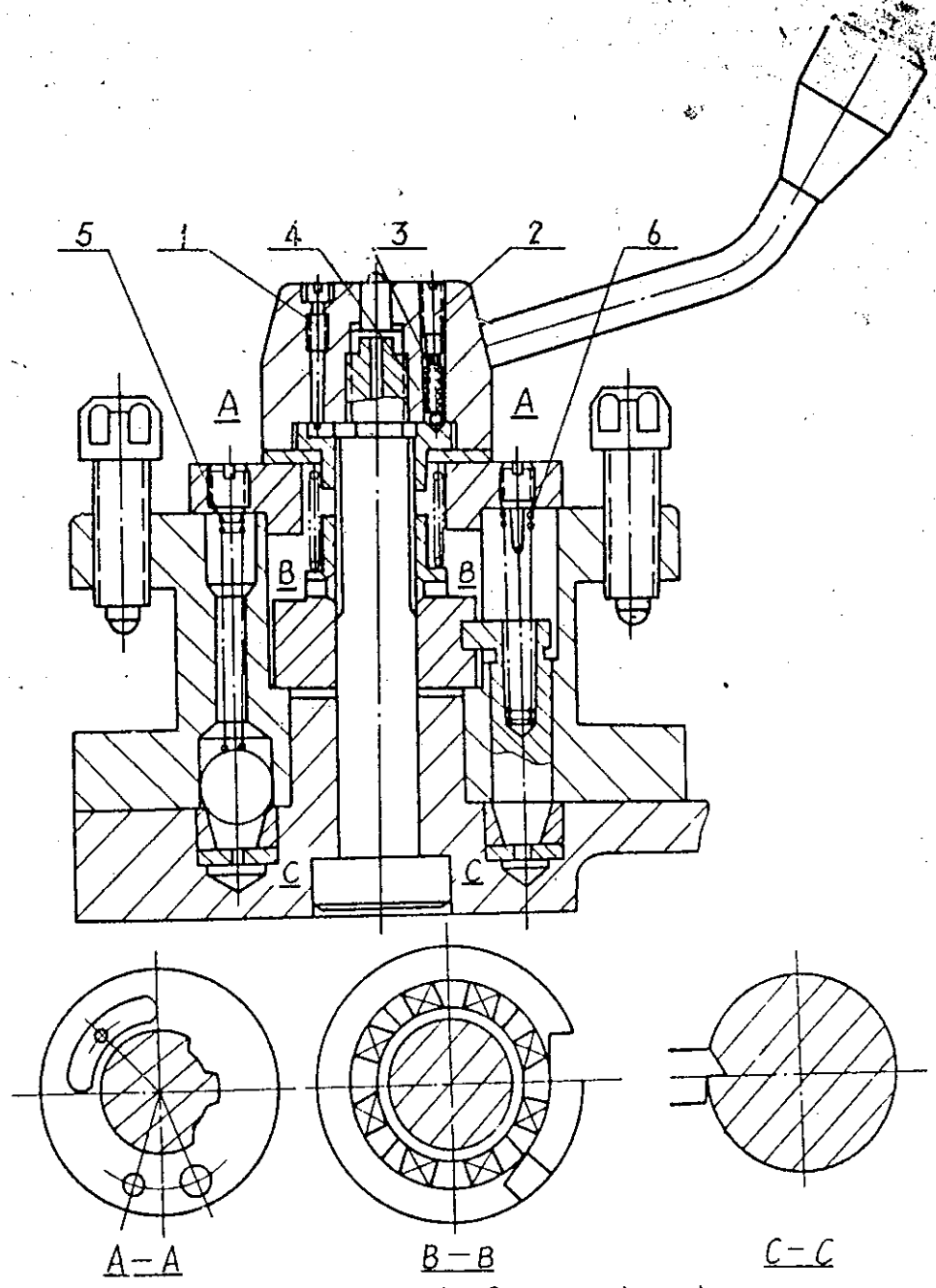


Fig.19 Construction sketch of square turret

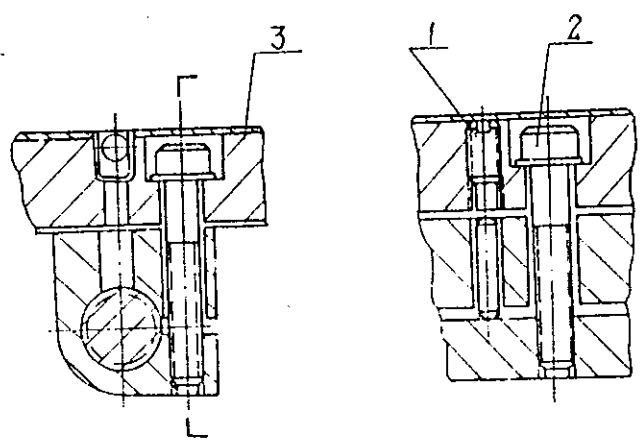


Fig.19 Adjusting diagram of screw nut in cross slide

编	产品型号	第 35 页
制	文件代号	共 61 页
	SY-AG-t	
日期		

is being stopped.

Under the condition that the cutting force and the feeding force can't approach the maximum allowable value specified by this machine, the adjusting screw 2 can be used in adjusting the overload clutch after the guard cap 1 is removed. (Fig.21). Care should be taken not making the clutch too tight, or otherwise it may lose the effectiveness for safeguard and cause machine parts to be damaged.

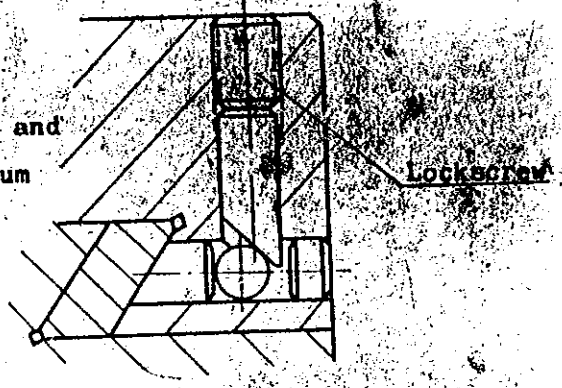


Fig.20 Diagram for locking devices of cross slide and top slide guide ways

An automatic mechanical interlocking device is set up between the longitudinal-transverse travel control-axle and the split-nut control-axle so as to prevent the leadscrew and the feed shaft from driving the apron simultaneously.

6. Feed box

The feed box provides with a specially designed "sliding gear mechanism", a thread variety change device and a multiply gear-ratio device to enable cutting common-used threads in inch, metric, diametral pitch or module without any effort of changing gears.

For ensuring the pitch accuracy of threads to be cut, the axial play of the leadscrew should be eliminated, the lock nut 1 can be used to adjust the thrust bearings 2 and 3. (Fig.22).

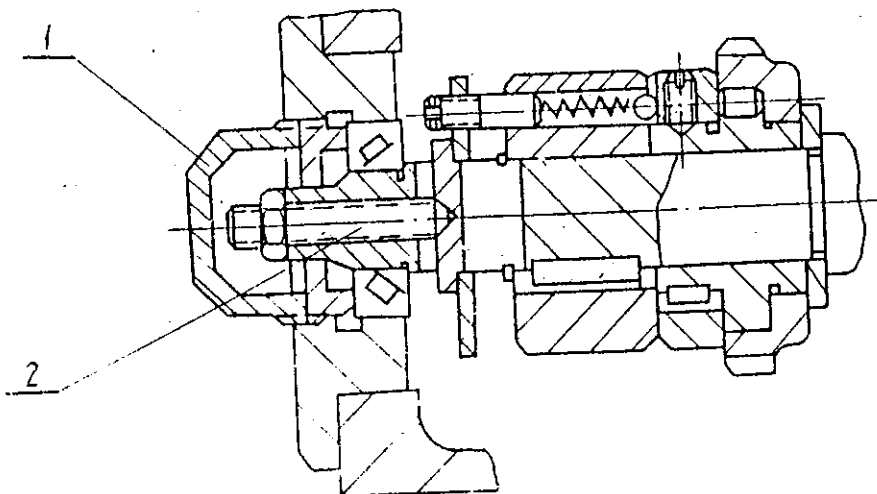


Fig.21 adjusting diagram of overload clutch

产品型号	SY-AB-7	第 36 页
文件代号		共 61 页
编 制		
日期		

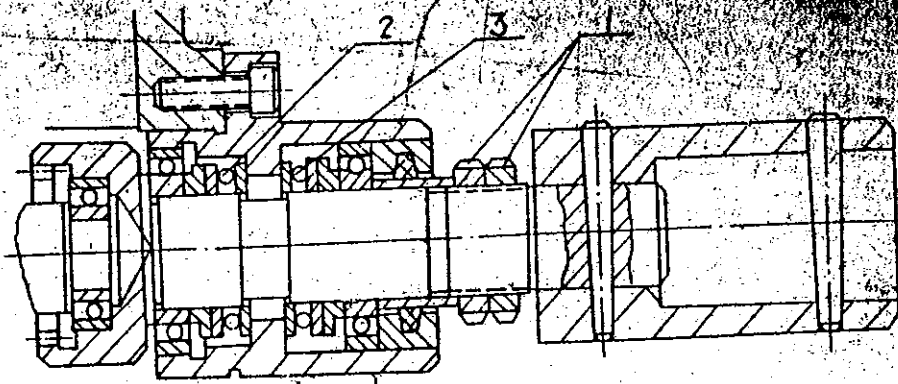


Fig.22 Adjusting diagram of thrust bearings on leadscrew

7. Transposing gears holder

In most cases of thread-cutting it needs not to change the primary transposing gears which have been fitted on the quadrant by the left side of headstock. Only when workpieces of threadpitch 19 or $11\frac{1}{2}$ teeth per inch being cut, it is then necessary to change and arrange them in accordance with the diagram shown in Fig.23. At that time, loosen idle axle 3 and remove it with nut 2, change the relevant gears accordingly and tighten them, thereafter loosen nut 1, turn the quadrant to adjust the clearance of gears in mesh and retighten it.

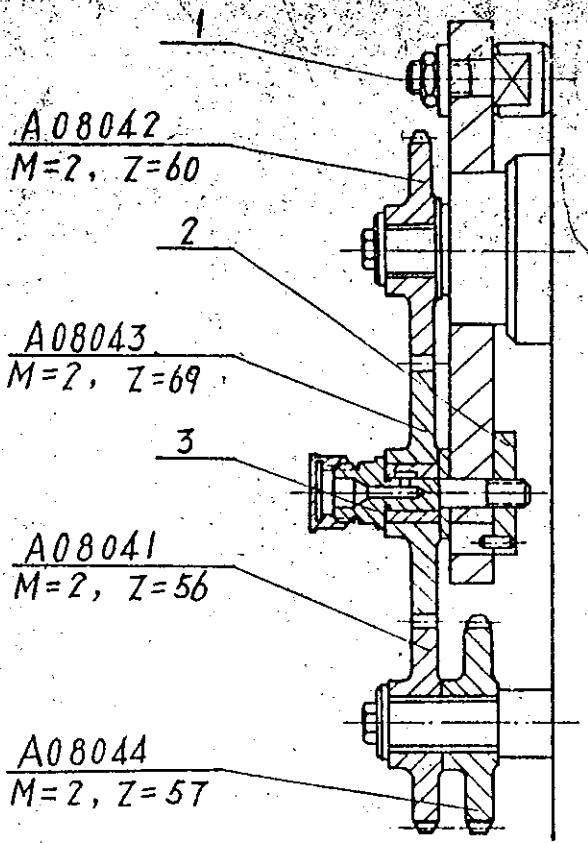
8. Chuck, driving plate, face plate and spindle nose

The chuck, driving plate or face plate is in connection with main spindle through spindle nose of camlock short taper flange type. To fit them over the spindle, the reference line engraved on each should be in alignment with the reference line engraved on spindle nose, and thereafter lock them firm by turning the cams on spindle flange in sequence and evenly. For the disassembling the above mentioned procedures are inversed. (Fig.24).

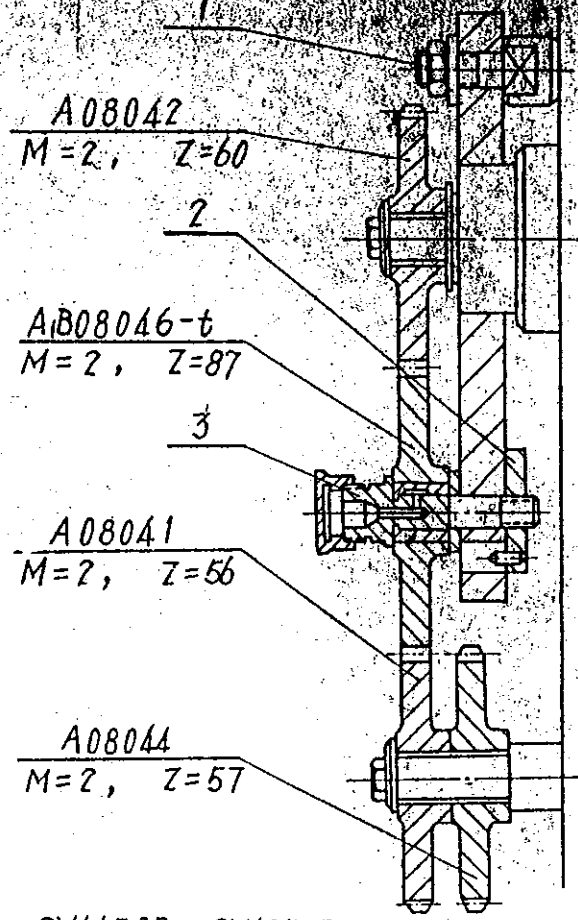
The sketch with dimension of spindle nose is shown in Fig.25.

9. For guards and cover plates of this machine a diagram about their dismantling is shown in Fig.26.

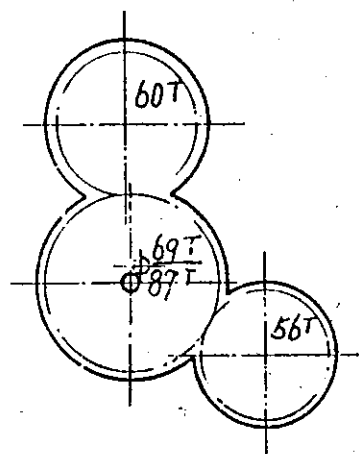
产品型号		家
文件代号	SY-AB-7.	共 6.
编 制		
日期		



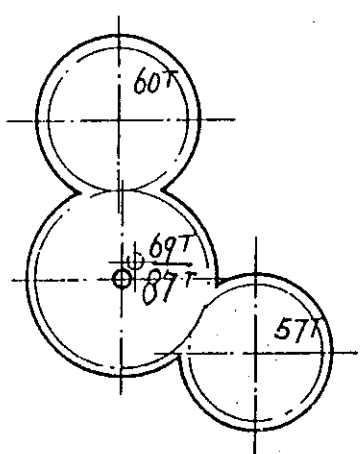
CY6140B, CY6240B



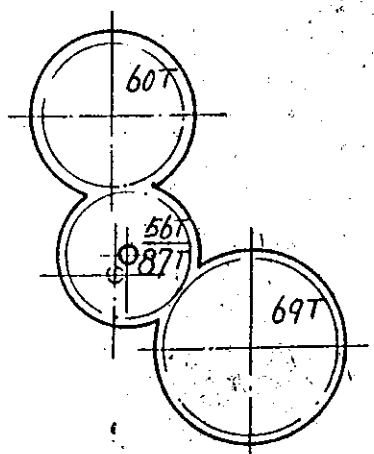
CY6150B, CY6250B



primary change gears



for 19 tpi



for 11½ tpi

Fig.23 Transposing gears for thread-cutting

产品型号	SY-A8-7	第 58 页
文件代号		共 61 页
编制		
日期		

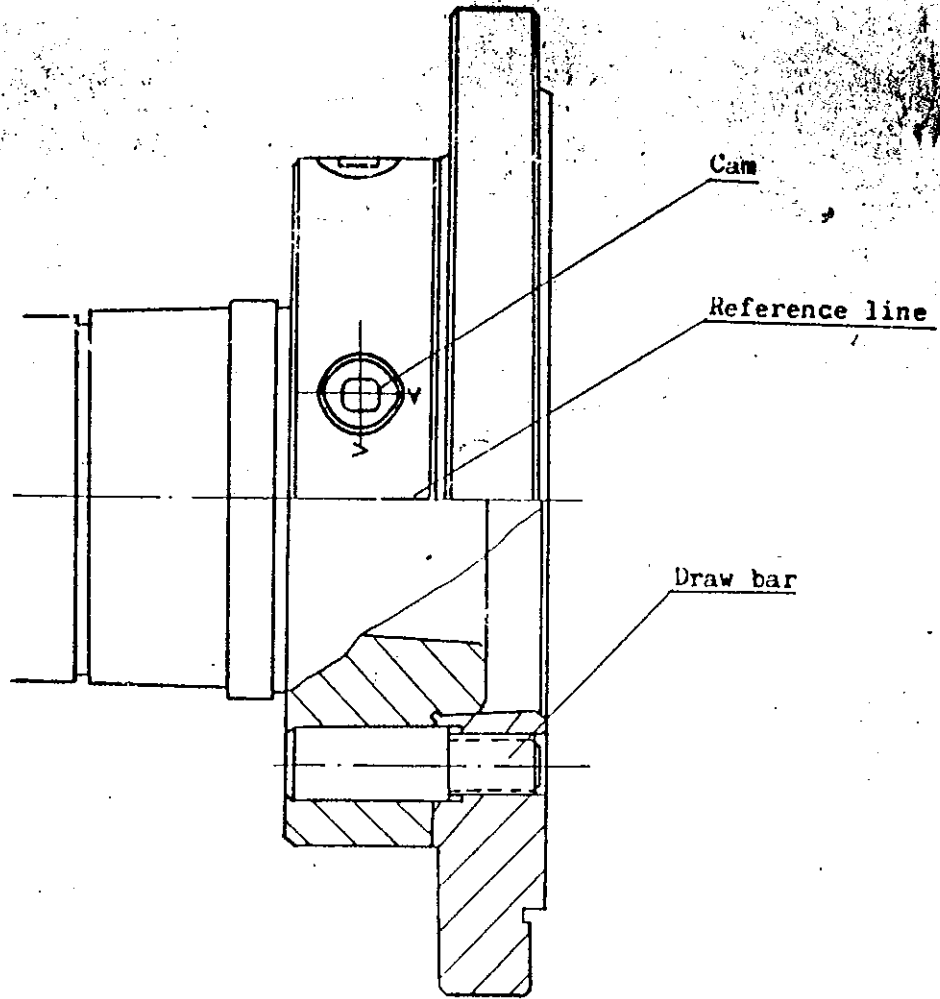


Fig.24 Assembly diagram for fitting chuck driving plate or face plate on spindle nose

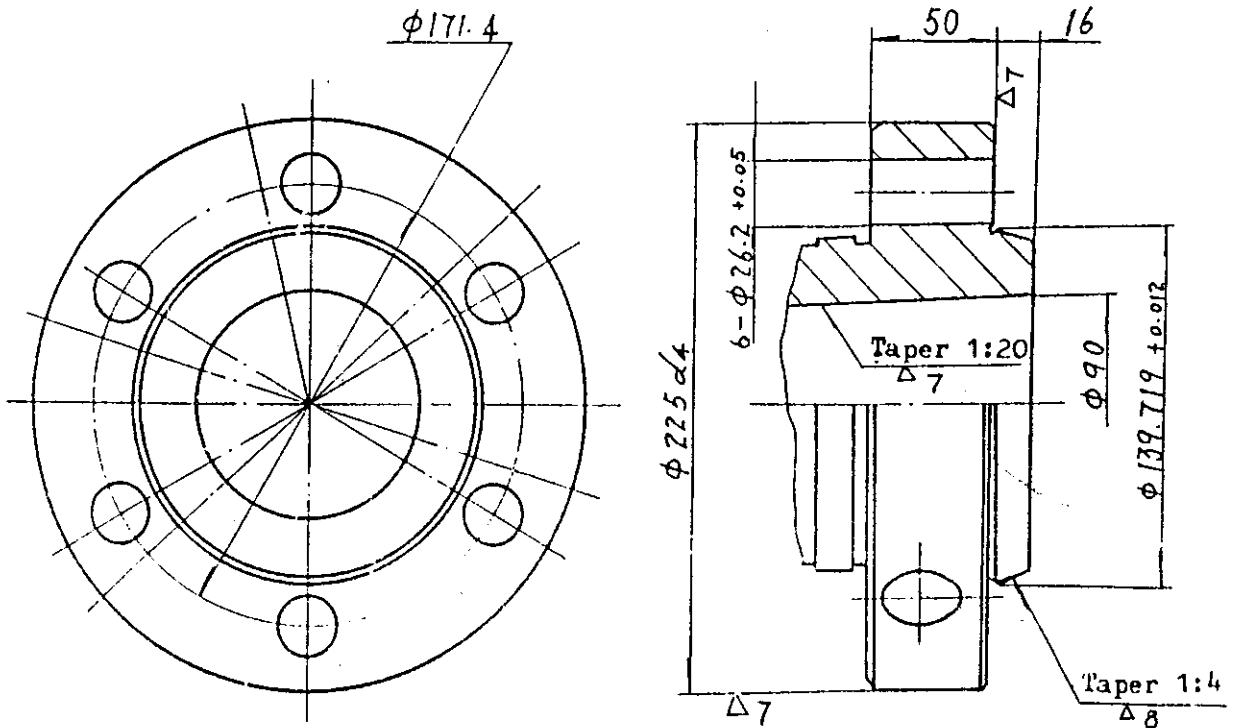


Fig.25 Diagrammatic sketch of spindle nose

产品型号	SY-AB-7
文件代号	第 59 页
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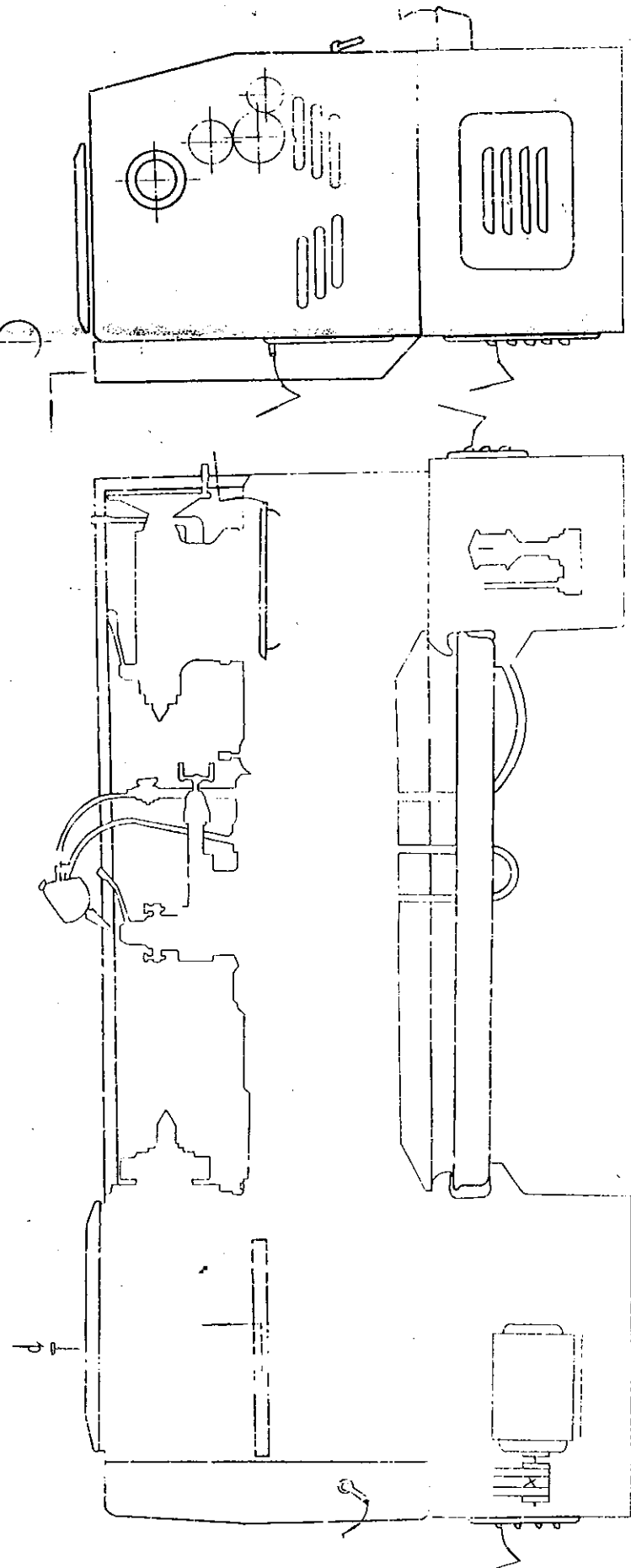


Fig. 26 Diagrammatic sketch about dismantling of guard and cover plates

X. Maintenance and service

1. Lubricating

For sake of ensuring proper operation of the machine and maintaining the original accuracy for precision performance in long periods, it is of vital importance that all the rubbing surfaces should be thoroughly cleaned in service and correctly lubricated on schedule so as to reduce the wear of machine parts and smooth the running and operating.

Please pay appropriate attention to the following suggestions:

(1) All lubrication points should be oiled according to the lubrication diagram before any cutting is attempted. The lubricants must be of a good quality and clean.

(2) For assuring sufficient lubrication the oil level in the boxes should reach to red line half way up on sightglass, but it should not be too high, otherwise the oil will leak out. So it needs to check the oil level frequently and add oil from time to time as required to maintain oil level when the spindle is not running.

(3) The lubricant in the headstock and apron must be renewed every 2-3 months. As the initial wearing value of new machine parts is greater, it is recommended that the first and second oil-change should be carried out after about ten working days and twenty working days respectively, thus the impurities may be removed in due time.

Please follow the procedure for oil-change:

1) Drain the remaining oil from the box;

2) Flush the inner parts in the box thoroughly with new kerosene;

3) Refill with fresh oil up to the oil level mark.

(4) Filter in the headstock, capillary woolen yarns and filter-felts at other lubricating sites should be thoroughly cleaned once a month. Dust-proof felts at both ends of the lower bedways of saddle and the right end of the tailstock base plate have to be washed with kerosene once every week. Change the worn felts as soon as being found.

2. Operating:

Pay close attention to the following suggestions during operating:

(1) After the main motor is started, check the working condition of the oil pump first through the oil window of headstock. Only when oil appears in the window, the spindle may be started.

(2) In order to avoid damages of the gears in headstock, the gear shifting levers should be put in their correct catch position. It must be checked before starting the main spindle by the operator.

(3) Changing the speed of main spindle can only be done when the spindle stops rotating. In any case the gear shifting levers should not be actuated.

编	文件代号	产品型号
制	SY-AG-7	
日期		
	共 61 页	第 41 页

when the spindle is in rapid revolution.

Changing the feedrates can be done in low speed condition or in a stop condition of main spindle.

(4) If the brake in headstock is out of order, it should be adjusted or repaired in time. Don't use the reverse friction clutch instead of the brake for stopping.

(5) When actuating the main spindle forward-brake-reversing lever in operation, the lever must be pulled or pressed to the proper position. It is not allowed to do speed-down cutting when the lever is not yet brought into position.

3. On use of the machine

For maintaining the service life and machining accuracy of the machine the following points are noteworthy:

(1) Check and adjust the tension of the V-belts at regular intervals for lengthening their service life.

(2) Clear away the dirt and coolant-contamination between the square turret and the top slide periodically to maintain the accuracy of location.

(3) When the quill taper bore of tailstock is used to hold the tool for cutting (such as spiral bohrers, reamers etc.), tool of M.T.No.5 taper shank with tang should be selected, and the tang has to be plugged levelly close against the stopper in the sleeve so as to prevent the tool from rotating in operation and injuring the finished surface of taper bore.

(4) The long leadscrew is used only for thread-cutting. For maintaining its accuracy and prolong the service life, it is not allowed to use the leadscrew instead of feed shaft for longitudinal feeding.

Besides, as the leadscrew drives the apron directly when cutting threads and the overload clutch in the apron is then no more a safeguard in this operation, for avoiding damages of the machine parts, the cutting depth in thread-cutting should be attentively considered so as to keep the feeding force P_x from ever exceeding 3400N.

(5) When the steady rest and/or the follow rest as well as the attachments (taper copy rule, thread chasing dial, stoppers etc.) are used in operation, their contact surface in rotating should be oiled accordingly.

编 号	产品型号	SY-AB-7	日期	第 44 页
	文件代号			共 51 页

XI. Attachments and tools

1. Attachments

A. Standard attachments are listed in Table 6.

Table 6 Details of standard attachments

Symbol	article	Specification	Qty	Remarks
AB09100-1	Three-jaw scroll chuck with backplate	250	1set	
AB09100-2		320	1set	
AB09200	Driving plate	250	1set	
A ₂ B09300	Four-jaw independent chuck with backplate	400	1set	for CY6240B and CY6250B
A ₂ B09400	Face plate	630	1set	for CY6240B and CY6250B
A10100	Steady rest	20 - 130	1set	for CY6140B and CY6240B
A ₁ 10100	Steady rest	20 - 130	1set	for CY6150B and CY6250B
A10200	Follow rest	20 - 80	1set	for CY6140B and CY6240B
A ₁ 10200	Follow rest	20 - 80	1set	for CY6150B and CY6250B
AB02403	Center sleeve		1pc	
S77-1	Center	M5	2pcs	

B. Optional attachments includes:

- Single-tool top slide,
- Taper turning attachment,
- Chasing dial (Thread dial indicator),
- 4-position carriage stopper,
- 4-position cross slide stopper,
- Micrometer carriage stopper,
- Automatic length stopper.

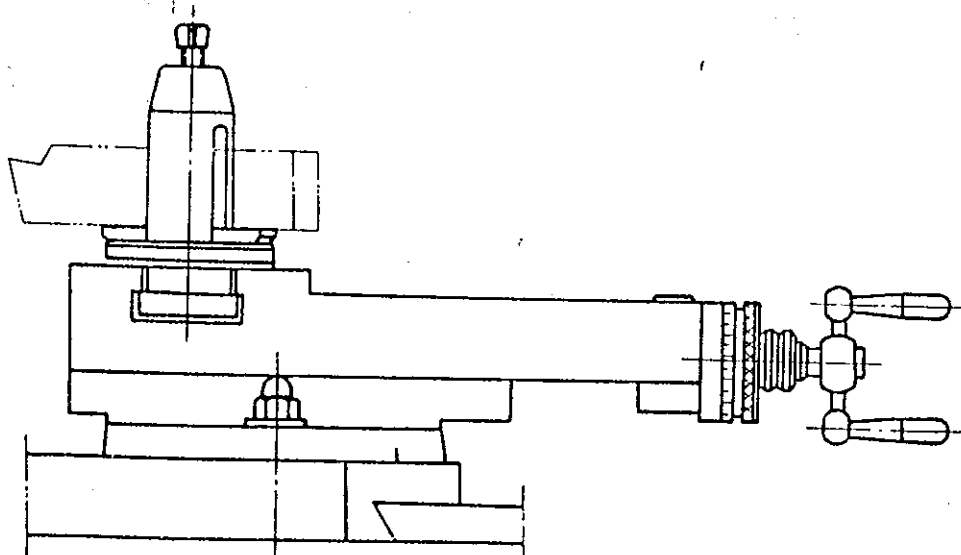
产品型号	
文件代号	SY-A8-t
共 43 页	第 41 页

A₁B04000/1 Single-tool compound rest

The single-tool compound rest is specially furnished for Universal Lathe CY6250B and Universal Gap-Bed Lathe CY6250B.

Dismount the square turret compound rest and fit this single-tool compound rest on cross slide, an American toolpost is then installed for application of turning tools with standard shank of cross section 19.05mm x 41.28mm.

The height from shank base plate to main spindle centerline is 37.5mm and the maximum travel of top slide is 146mm. (see sketch b below).



产品型号	
文件代号	SY-AR-7
第 44 页	共 11 页

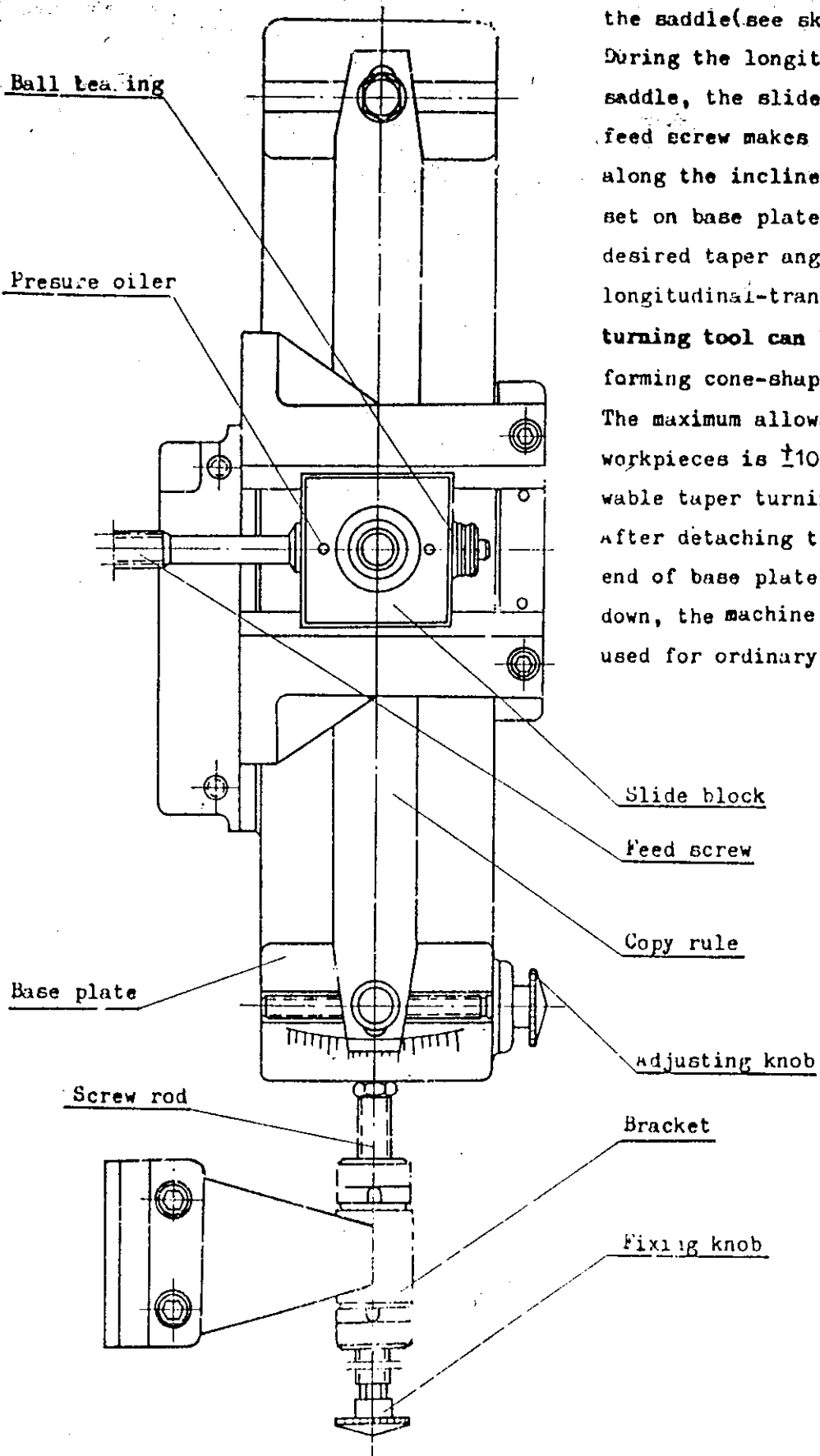
A312000 Taper turning attachment

This attachment is arranged at rear of the saddle(see sketch below).

During the longitudinal movement of saddle, the slide block connected to the feed screw makes a transverse motion along the inclined copy rule which is set on base plate in accordance with the desired taper angle. Thus a combined longitudinal-transverse movement of turning tool can be achieved for performing cone-shaped workpieces.

The maximum allowable taper angle of workpieces is $\pm 10^\circ$ and the maximum allowable taper turning length is 300mm.

After detaching the screw rod from the end of base plate and taking the bracket down, the machine is then still to be used for ordinary turning works.



产品型号	
文件代号	51-10-7
第 45 页	

AB21000 Chasing dial (Thread dial)

The chasing dial is set up on the right hand light side of the lathe. The dial is graduated in 15 divisions, since a complete circle of the dial represents 15 revolutions of the leadscrew, so that each division on dial equals one revolution of the leadscrew.

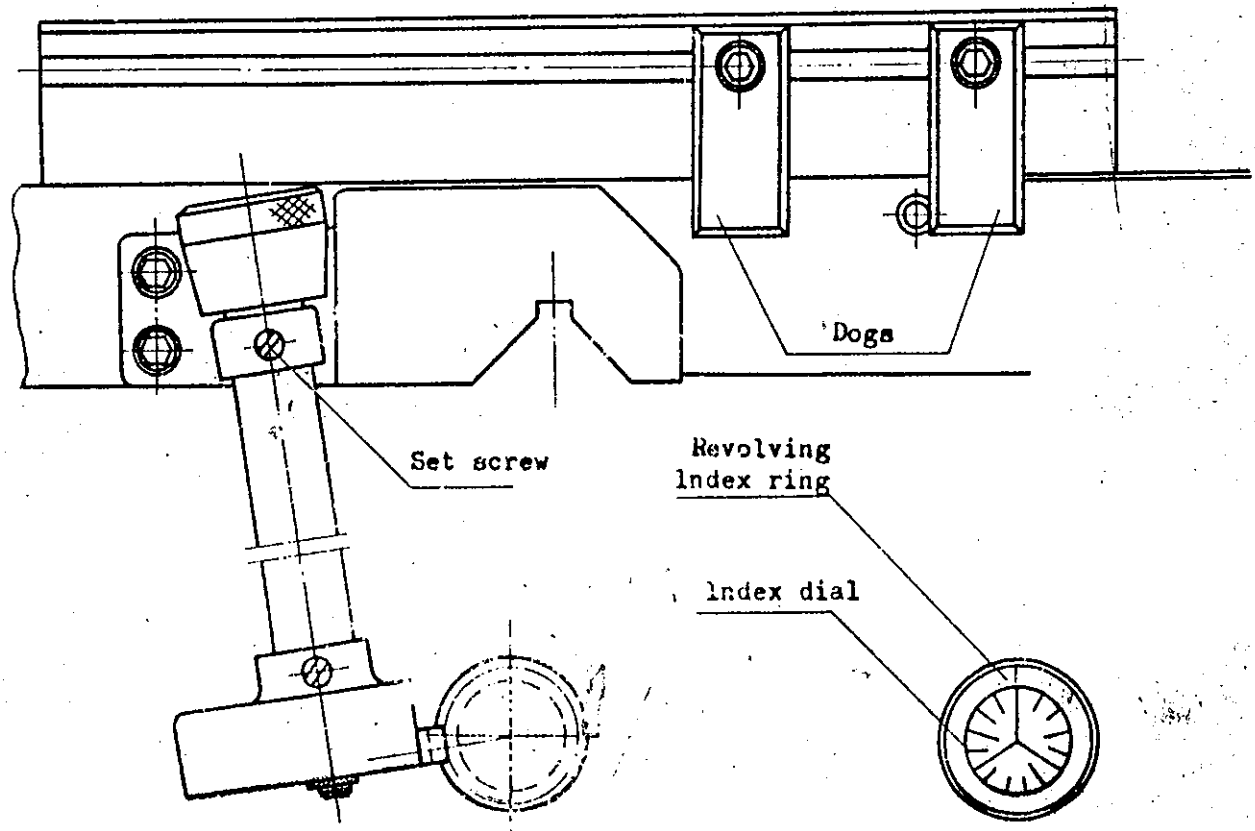
For getting an unbroken-thread in repeated cuts, each of the various metric threads listed in Table 2 can be cut easily and perfectly with the aid of chasing dial by taking the relevant index number y (or its multiples) in following table, where y represents the necessary number of revolutions of leadscrew to be indexed on dial whilst the split-nut disengages from the leadscrew:

Thread pitch (mm)	0.5	0.75	1	1.25	1.5	1.75	2	2.25	2.5	2.75	3	3.5	4	4.5	5	5.5
Index number y	1	1	1	5	1	—	1	3	5	—	1	—	1	3	5	—

Thread pitch (mm)	6	7	8	9	10	11	12	14	16	18	20	22	24	28	32	36
Index number y	1	—	—	3	5	—	1	—	—	3	5	—	—	—	—	3

The feed-in and draw-back of turning tool could be limited by means of the dogs preset on the right hand side of cross slide.

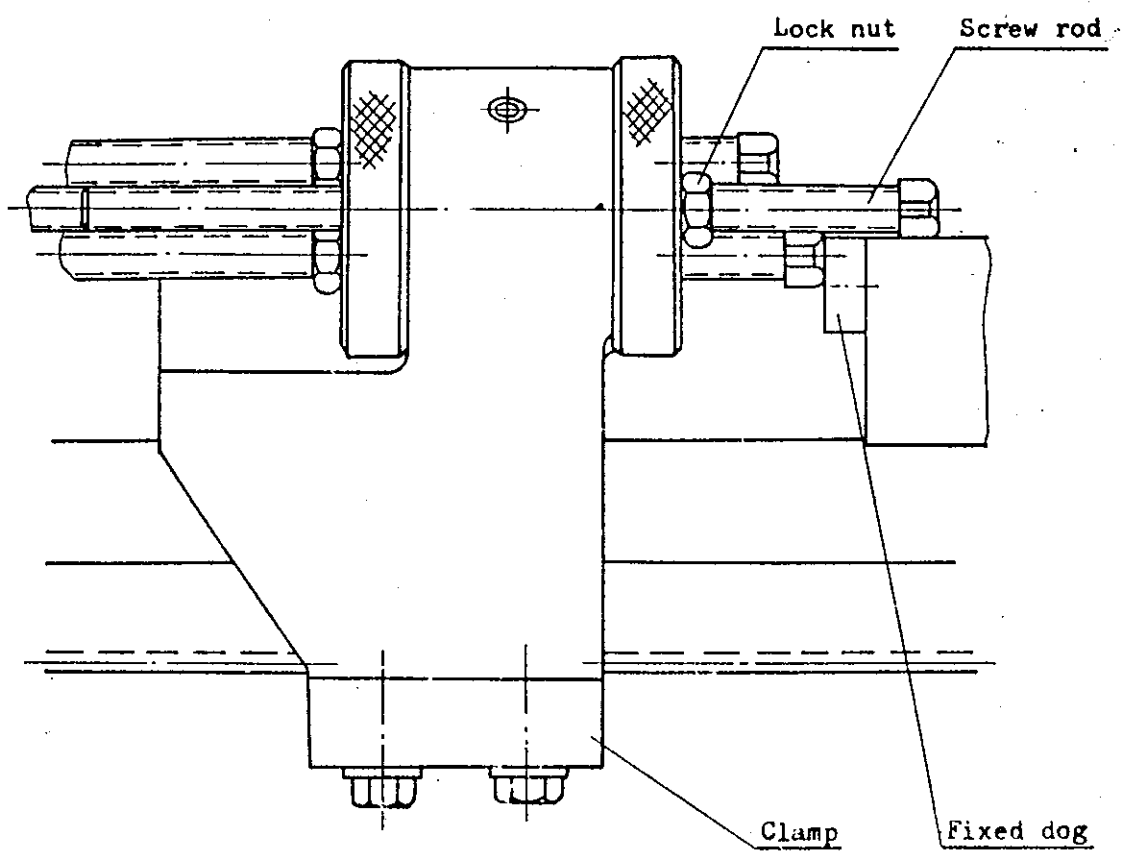
Having first loosen the set screw, the chasing dial could be lifted up and disengages from the leadscrew when the chasing dial is not in use.



产品型号	SY-48-t	第 46 页
文件代号		共 61 页
编制		

AB22100 4-position carriage stopper

The 4-position carriage stopper is mounted on the front bed-guidways by the left hand side of saddle and fastened by means of a clamp through its rack-teeth embedding into the bed-rack. It is used in producing batches of identical workpieces for avoiding loss of time through taking measurements, as each of the four adjustable stops may be set for a different position and may be revolved into position to locate the carriage for each of four successive cuts. The maximum adjustable length of each screw rod is about 125 mm.

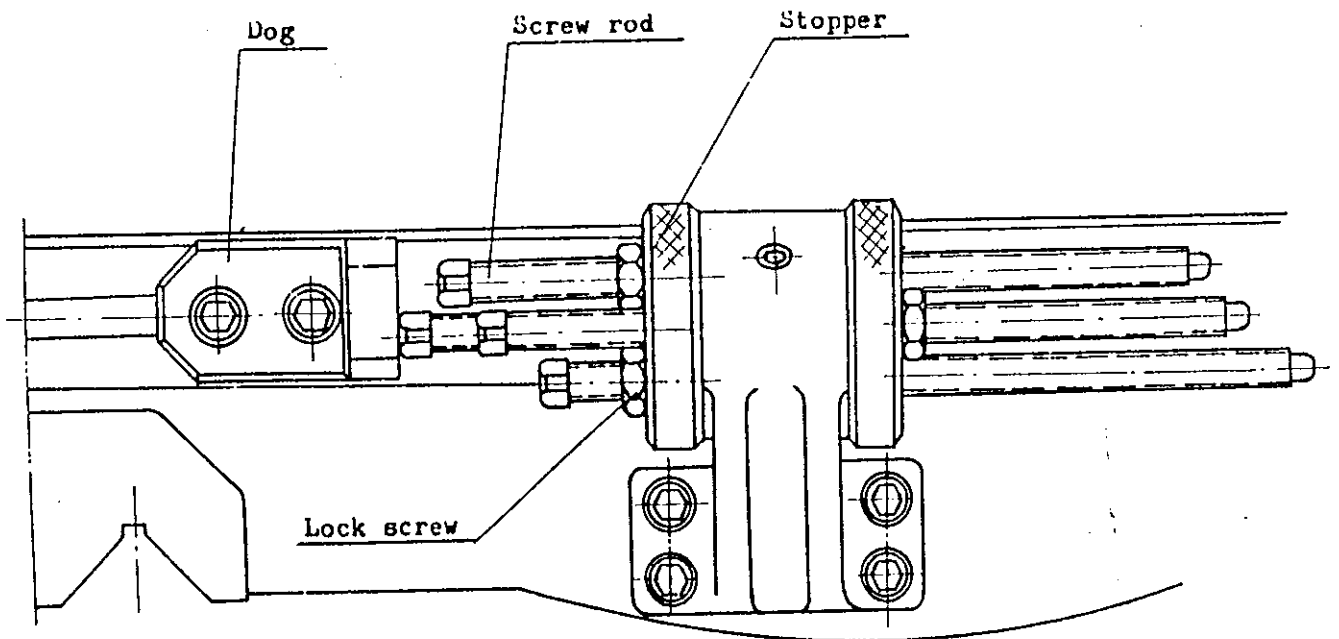


产品型号	
文件代号	SY-A6-6
第 47 页	
共 61 页	

AB22200 4-position cross slide stopper

The 4-position cross slide stopper is mounted on the right hand side of saddle, whereas the adjustable dog is fixed by screws along the T-slot on the right hand side of cross slide and moves with it together.

Four adjustable screw rods of stopper may be set for different cutting depths and may be revolved into position to locate the cross slide for each of four successive cuts. Thus, it is suitable to be used in batch production of identical workpieces. The maximum adjustable length of each screw rod is about 125mm.



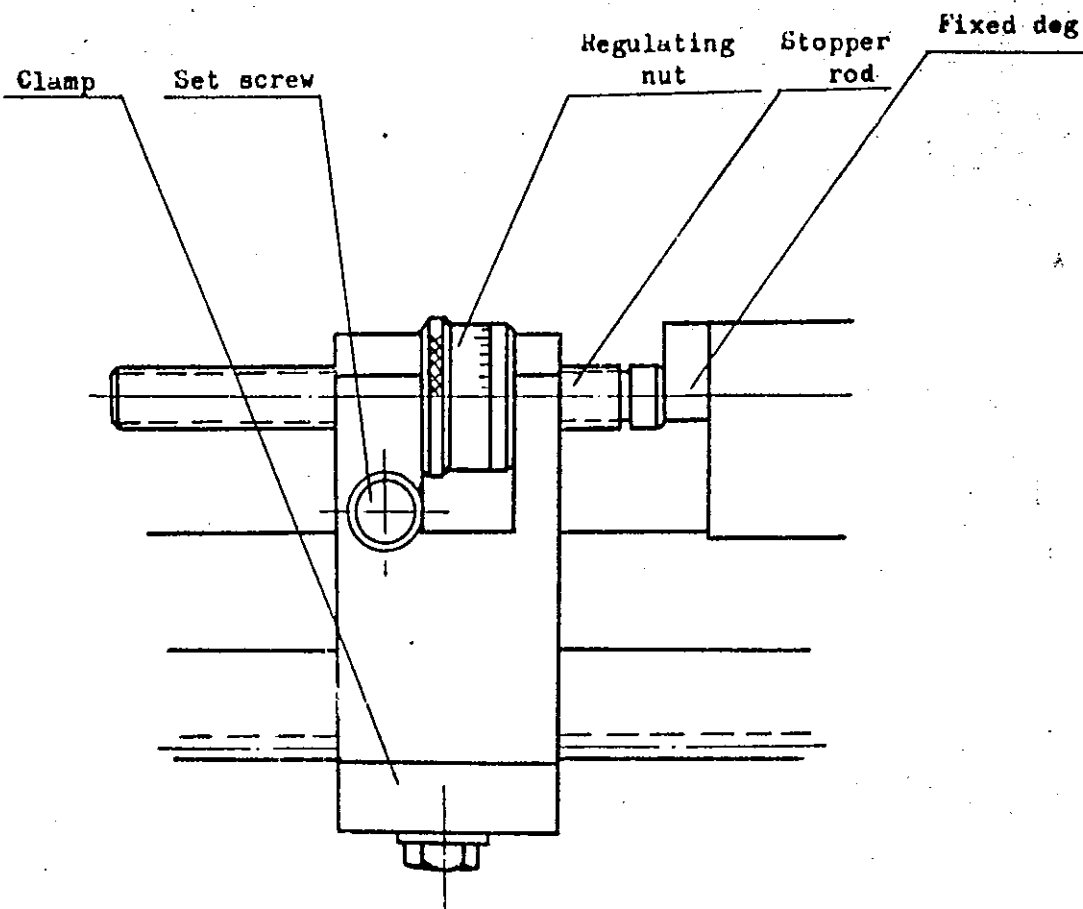
产品型号		第 48 页
文件代号	SY-A8-1	共 61 页

AB22500 Micrometer carriage stopper

The micrometer carriage stopper is mounted on the front bed-guideway by the left hand side of saddle and fastened by means of a clamp through its rack-teeth embedding into the bed-rack.

The threadpitch of stopper screw rod is 1mm and each division on the barrel of the round-nut for fine adjustment equals 0.02mm in length. The set screw is used to lock the screw rod after the adjustment is completed.

The maximum adjustable length of screw rod is about 125mm.

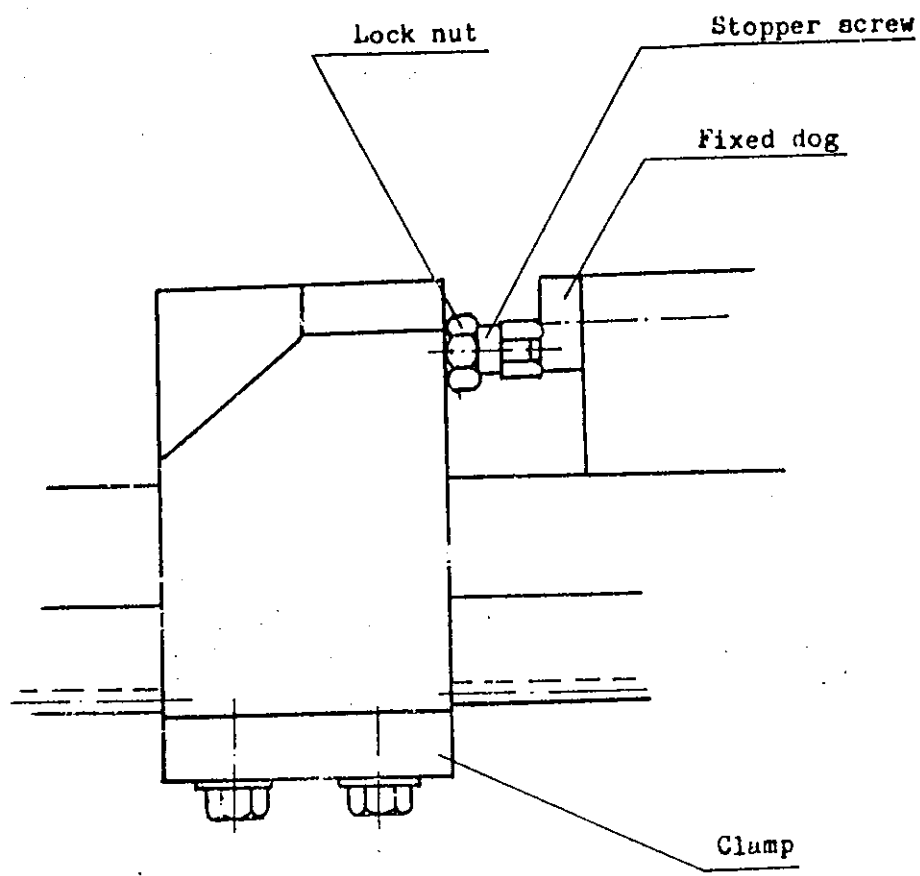


AB22600 automatic length stopper

The automatic length stopper is set up on the front bed-guideway by the left hand side of saddle and securely fastened by a clamp through its rack-teeth embedding into the bed-rack. The stopper screw has a length of 16mm for adjustment. As the saddle is being driven by the feed shaft and moving forward longitudinally until the fixed dog on left side of the saddle strikes the head of stopper screw, it causes an overload of the safety clutch in apron and shifts the power-feed lever returning to neutral position. A kick-off stop of automatic feeding is then performed.

When the power-feed lever is actuated for longitudinal travel again after a kick-off stop, it may sometimes happen that the lever could not be brought into the relevant position. This phenomenon would be eliminated at once merely by actuating the lever reversely to make the apron a starting-up.

The maximum kick force of stopper equals to the maximum permissible feeding force, i.e. 3400 N .



产品型号	
文件代号	SY-AB-7
日期	
共 61 页	第 50 页

2. Tools: The commonly used service tools are listed in Table 7.

Table 7 Details of commonly used tools

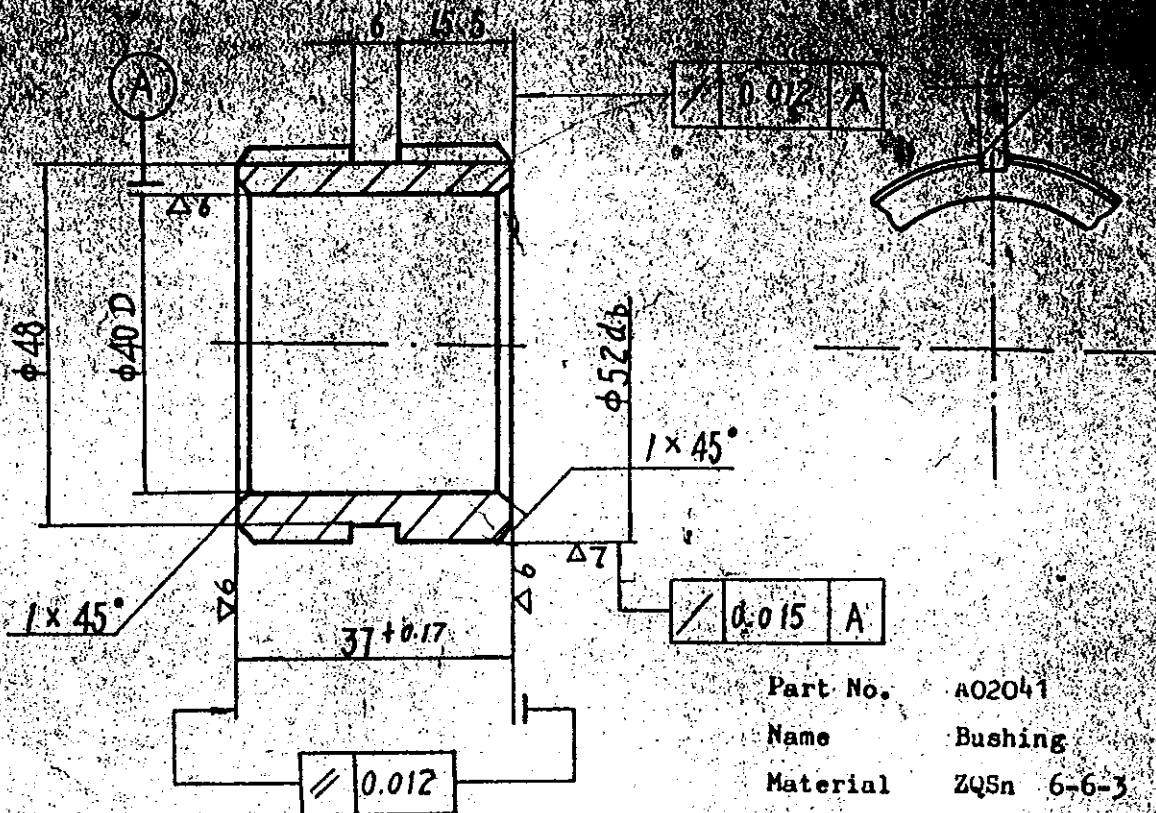
Symbol	Tool	Specification	Qty	Applications
AB13001	Knurled head shaft		1pc	Adjust the front lock nut of main spindle.
AB13002	Spanner	14	1pc	Mount the chuck, driving plate and face plate.
S91-1	Double-ended spanner	10 x 12	1pc	Fix the saddle. Adjust the rear plate of saddle, clamp the turning tool in single-tool tool post.
S91-1	Double-ended spanner	14 x 17	1pc	Adjust the rear pressure plate of saddle and the screw rod of cross slide stopper. Change the transposing gears.
S91-1	Double-ended spanner	19 x 22	1pc	Adjust the brake band, the rotary angle of swivel base on cross slide, overload clutch in apron and the screw rods of carriage stopper.
S91-1	Double-ended spanner	27 x 30	1pc	Fix the body of tailstock on base plate and steady rest on bed. Adjust the motor rest and transposing gears holder, change the transposing gears.
S91-7	Socket screw hexagon wrench	5	1pc	Fix the top slide and cross slide. Adjust the stop dogs for cross slide stopper.
S91-7	Socket screw hexagon wrench	6	1pc	Adjust the main spindle bearings and overload clutch in apron.
S91-7	Socket screw hexagon wrench	8	1pc	Adjust the main spindle bearings and the screw nut of saddle, dismantel the cover plate of headstock.
S91-7	Socket screw hexagon wrench	10	1pc	Adjust the set-over of tailstock. Dismount the gap block.
S91-7	Socket screw hexagon wrench	12	1pc	Dismount the gap block. Fix the follow res
S92-3	Square socket wrench	17	1 set	Clamp the turning tools in square turret.
S93-1	"C" Spanner	45-48	1pc	Adjust the axial clearance of leadscrew. Fix the nuts of screw rod in bracket of taper turning attachment.
S93-1	"C" Spanner	135-165	1pc	Adjust the main spindle bearing.
CB1165-74	Oil gun	100c.c.	1pc	
	Screw driver	150	1pc	Adjust the springs of clutch, tension wheel of chain and gib screws etc.

编 产品型号
 制 文件代号
 日期 59-AG-7
 共 61 页
 第 51 页

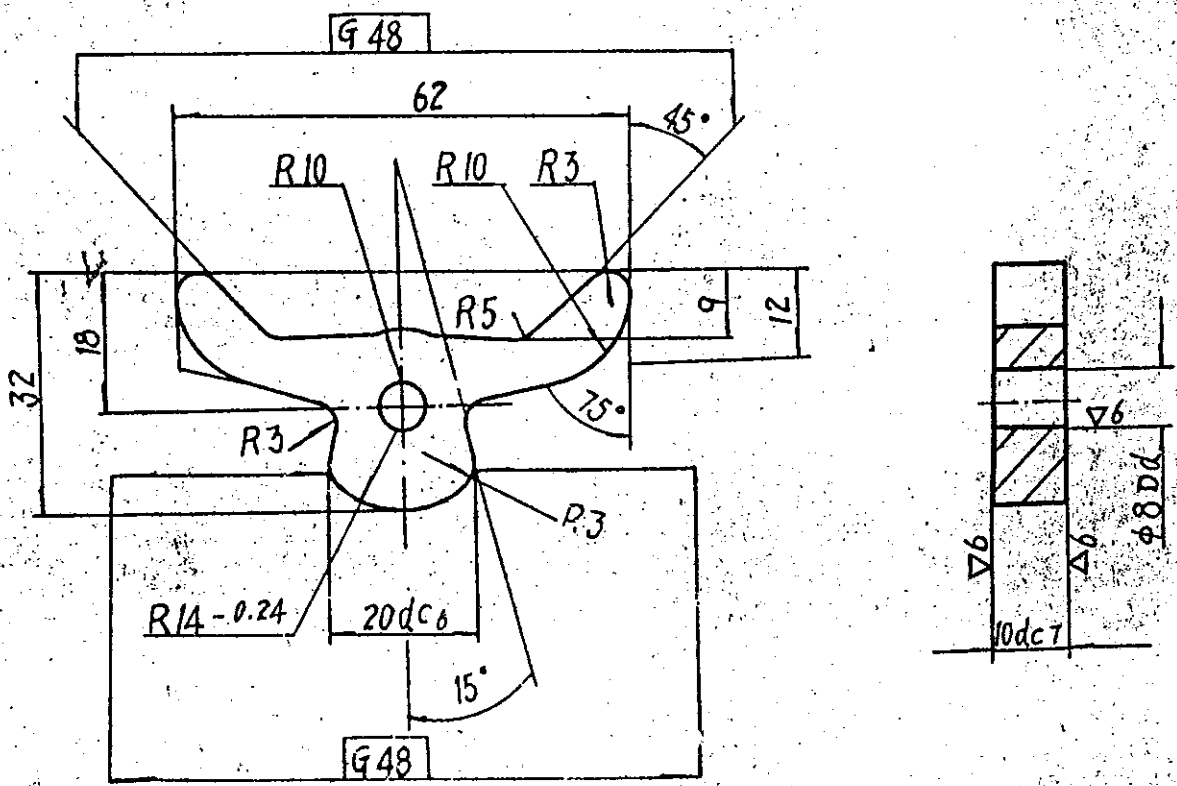
Table B: Details of easy worn parts

Seral No.	Part number	Part name	Material	Heat treatment	Qty
1	A02041	Bushing	ZQSn 6-6-3		2pcs
2	A02136	lever	45	048 locally	1pc
3	A02192	inner disc of clutch	15	So.5-C60	16pcs
4	A02193	Outer disc of clutch	15	So.5-C60	14pcs
5	A02194	Brake band	65 Mn		1pc
6	A02211	Outer rotor of trochoid pump	Sintered powder iron basic metal		1pc
7	A02212	Inner rotor of trochoid pump	Sintered powder iron basic metal		1pc
8	A02231	Brake friction plate	Canvas with iron sand		1pc
9	A 05011	Slide nut	ZQSn 6-6-3		1pc
10	A06021-R	Worm wheel	ZQSn 6-6-3		1pc
11	A 06022	Split-nut	ZQSn 6-6-3		1pc
12	A08011	Splined bush	ZQSn 6-6-3		1pc
13	J22-1	Screw M16 x 40	35		8pcs
14	Q99-1, 12	Slide block	HT 20-40		1pc
15	Q99-1, 16	Slide block	HT 20-40		1pc
16	S77-1, M5	Center II-MT5	T8	tip C59 shank C40	1pc

产品型号	文件代号	编制日期	共 61 页
	SY-AB-R		第 51 页



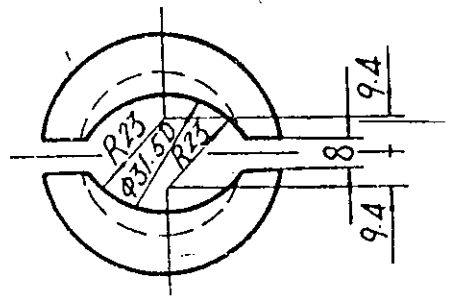
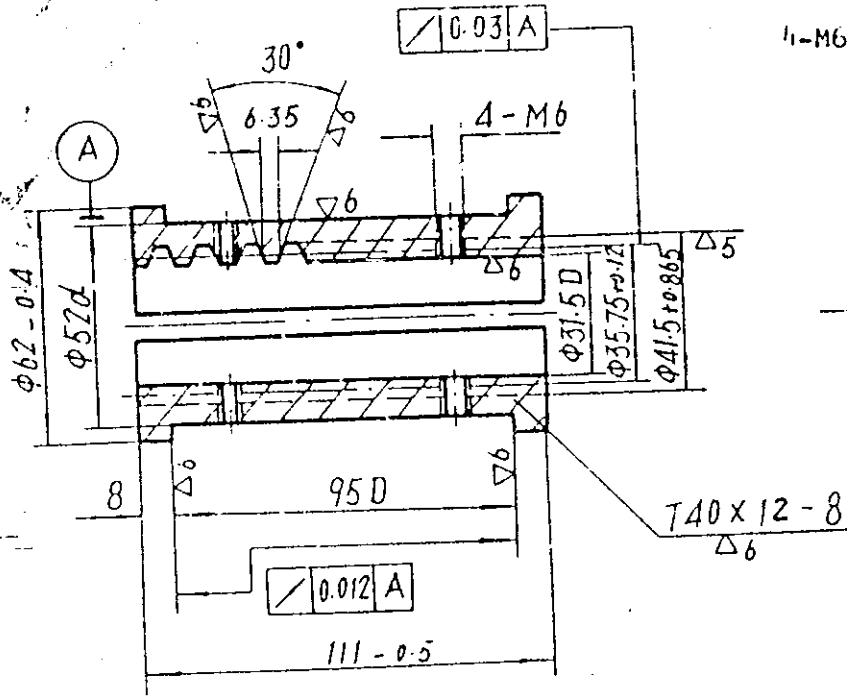
Others $\nabla 4$



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文件代号	SY-A8-7
日期	
共 61 页	
第 53 页	

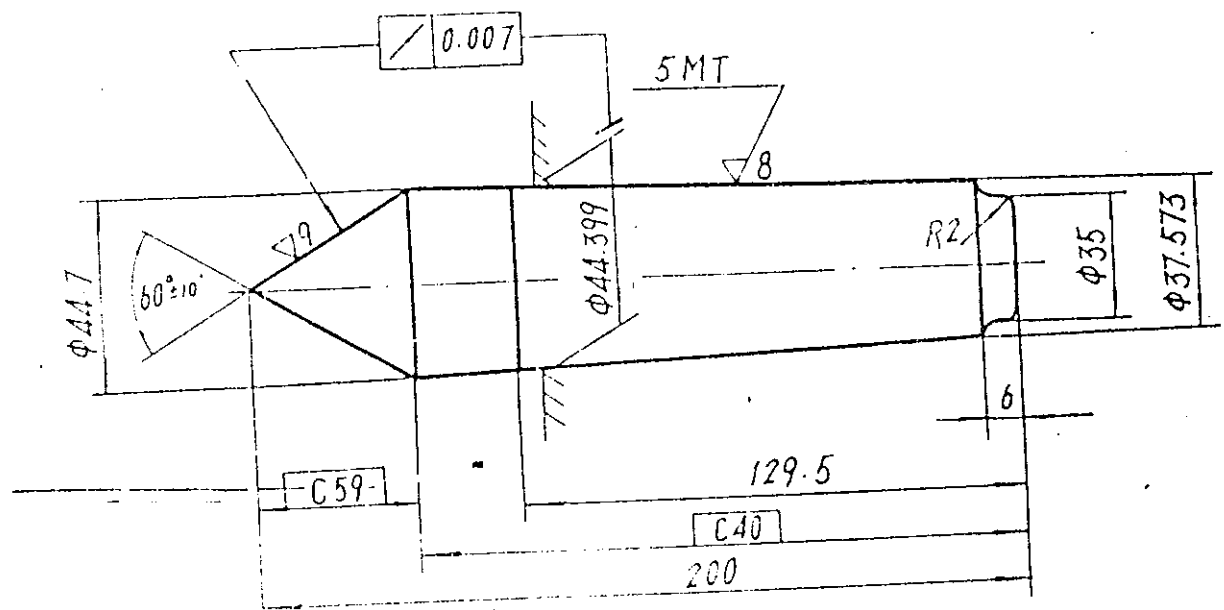
Others $\nabla 4$

4-M6 Making; with the holder

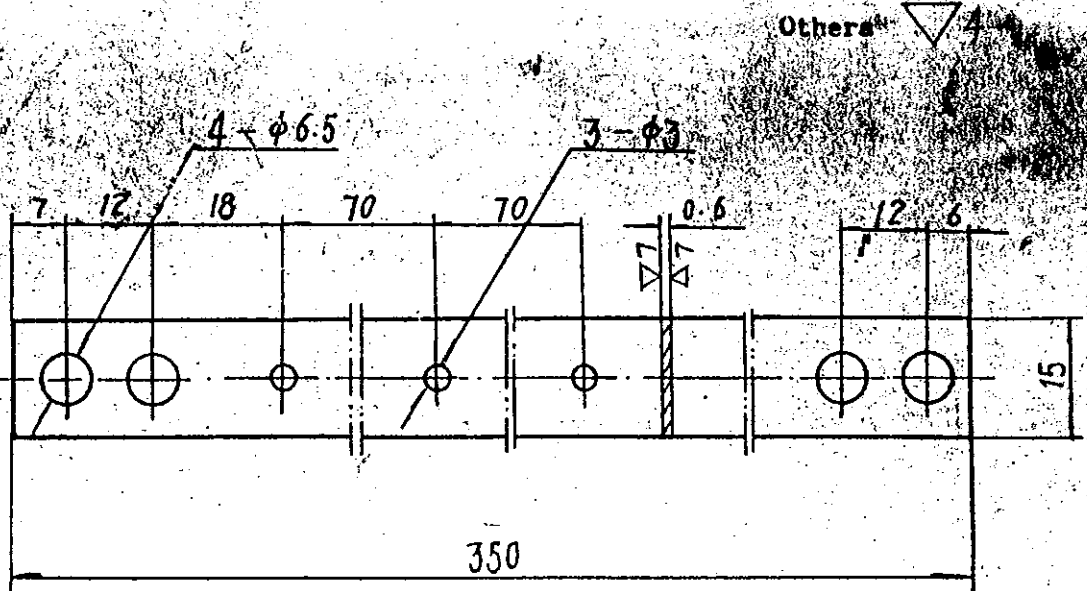


Part No. A 06022
 Name Split-nut
 Material ZQSn 6-6-3

Others $\nabla 5$



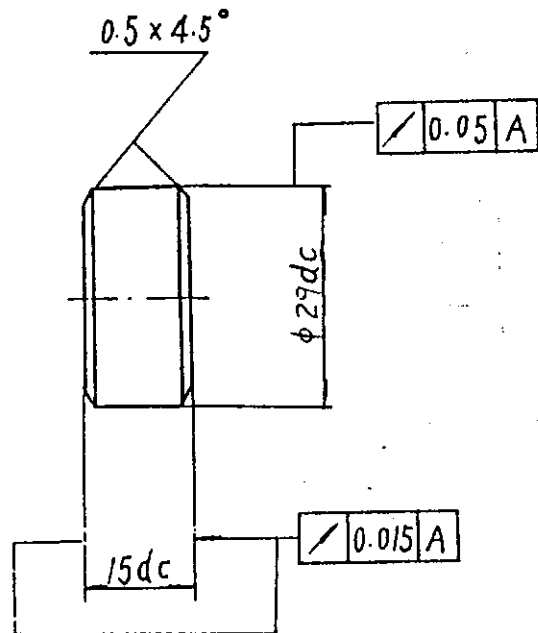
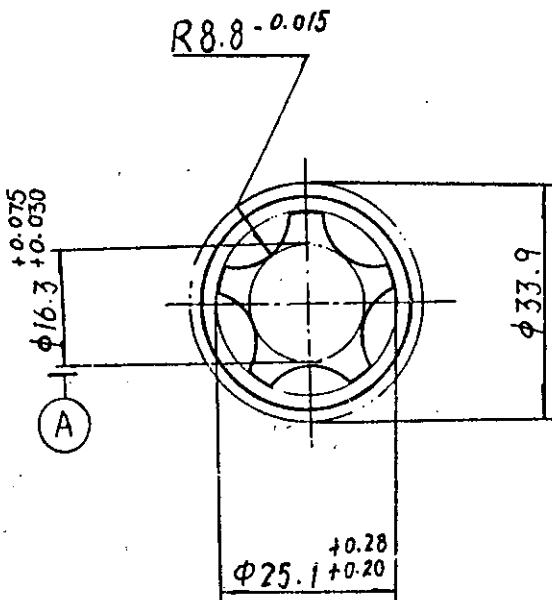
Symbol 577-1
 size 5MT
 Name Center
 Material T8



Part No. A02194
 Name Brake band
 Material 65 Mn

Parameter: $e=2.2, a=8.8 R=16.95, z=5$


Total $\nabla 6$

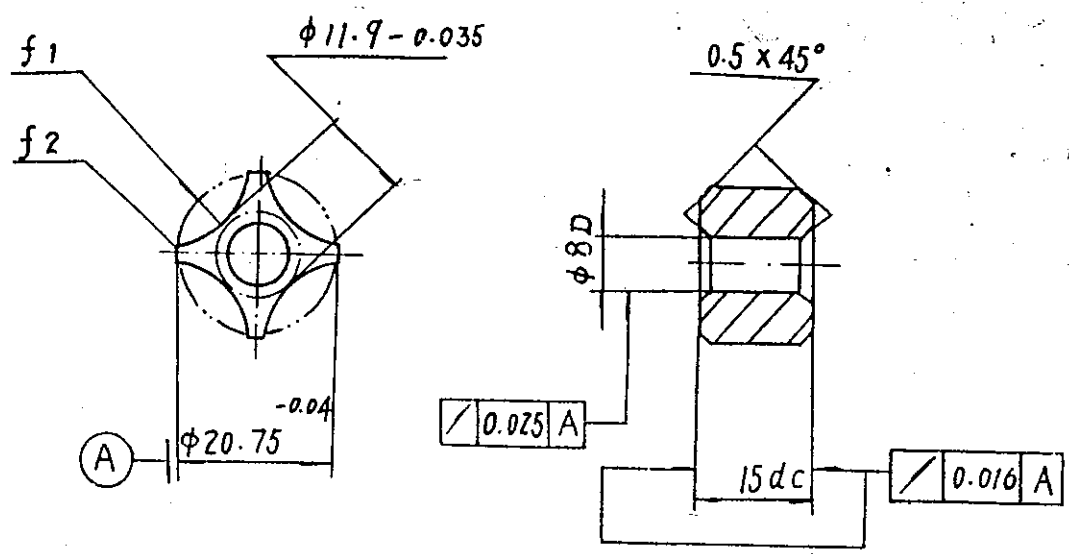


Part No. A02211
 Name Outer rotor of trochoid pump
 Material Sintered powder iron basic metal

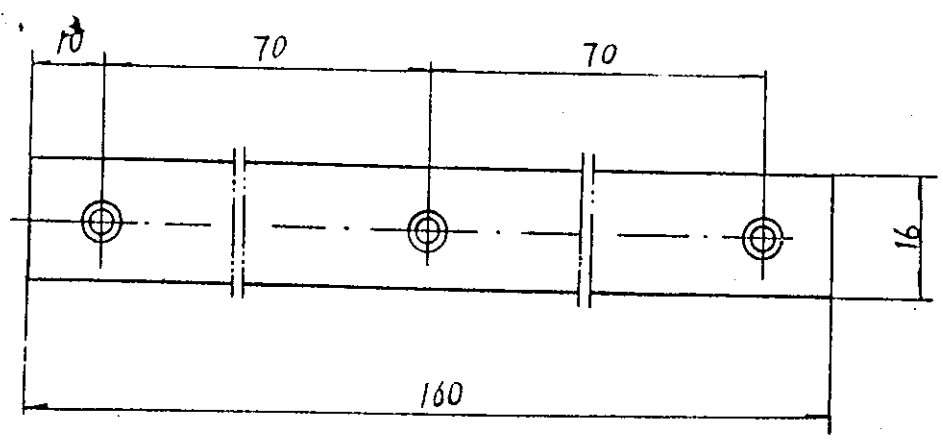
编	产品型号		第 55 页
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	日期		

Parameter: $e=2.2$; $R=16.95$; $a=8.8$; $z=4$.

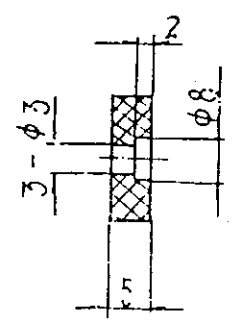
Total 



Part No. A02212
 Name Inner rotor of trochoid p
 Material Sintered powder iron basi
 metal

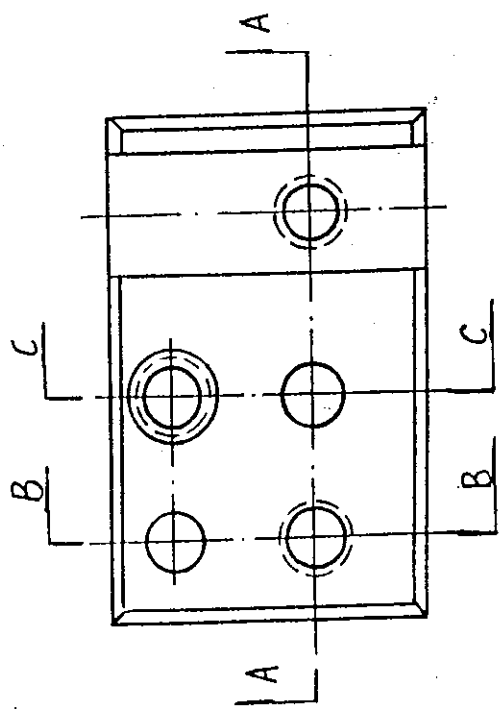
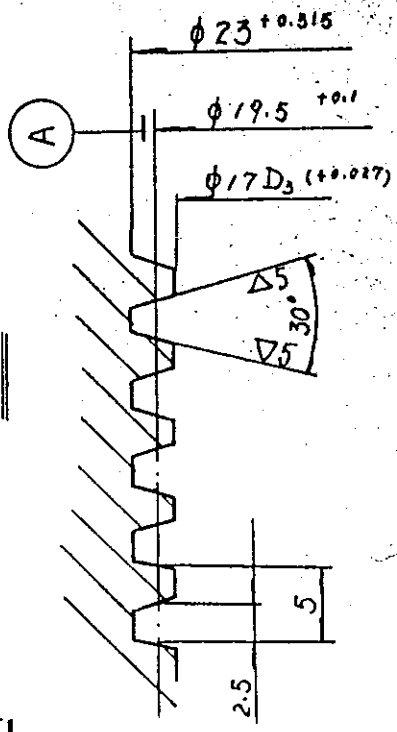
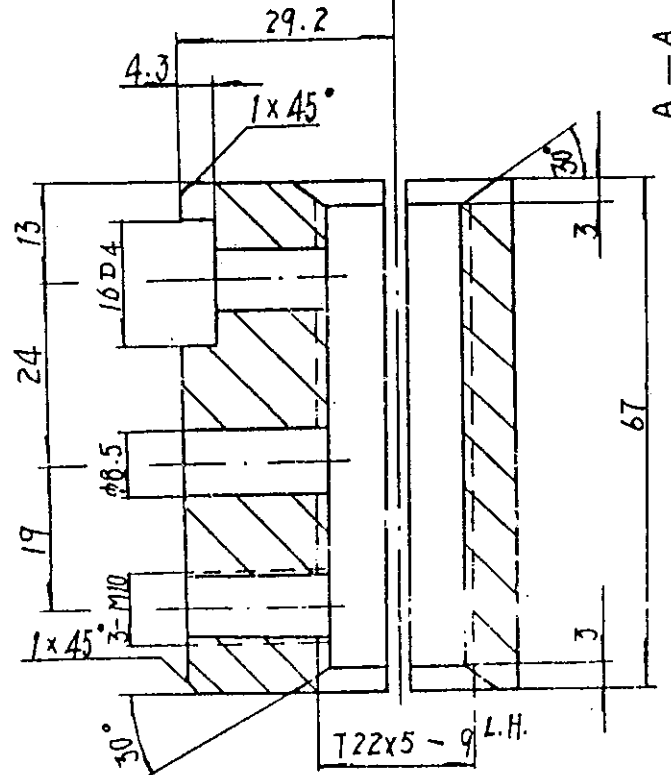
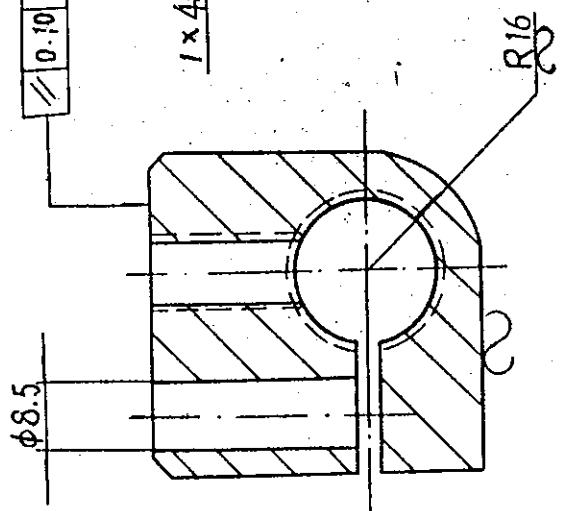
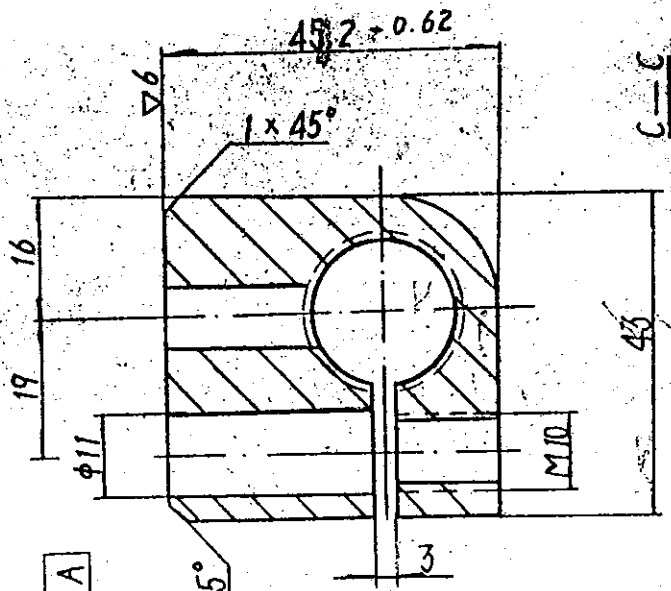


The cutting edges should be smooth and fl



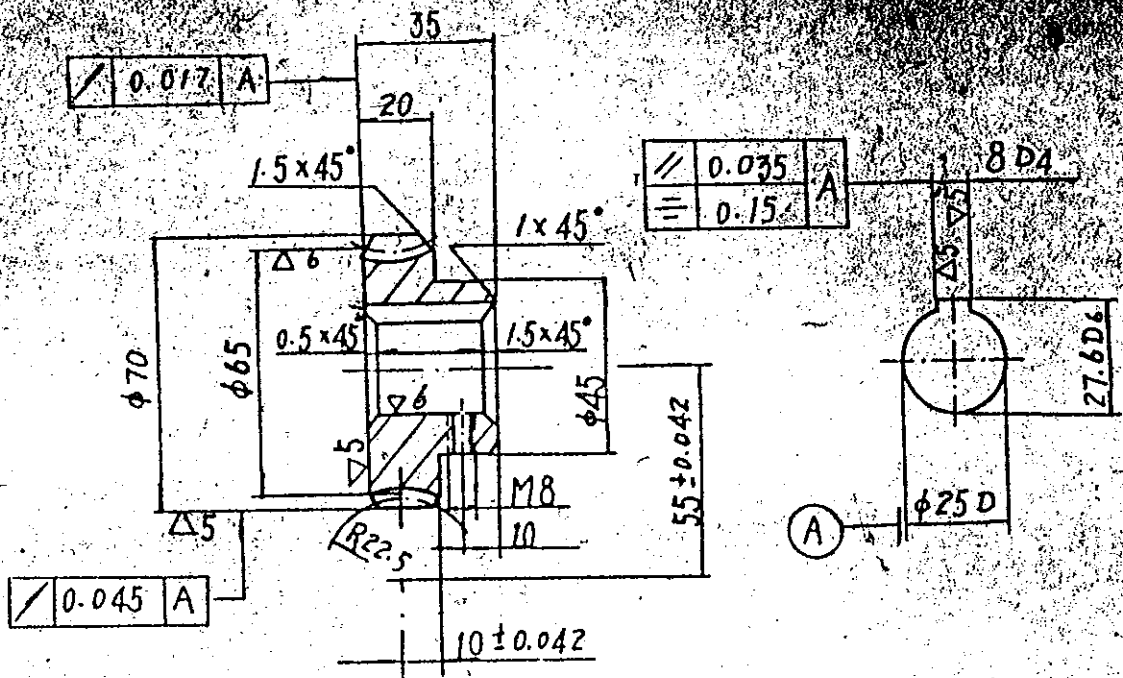
Part No. A02231
 Name Brake riction plate
 Material Canvas with iron sand

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		共 61 页



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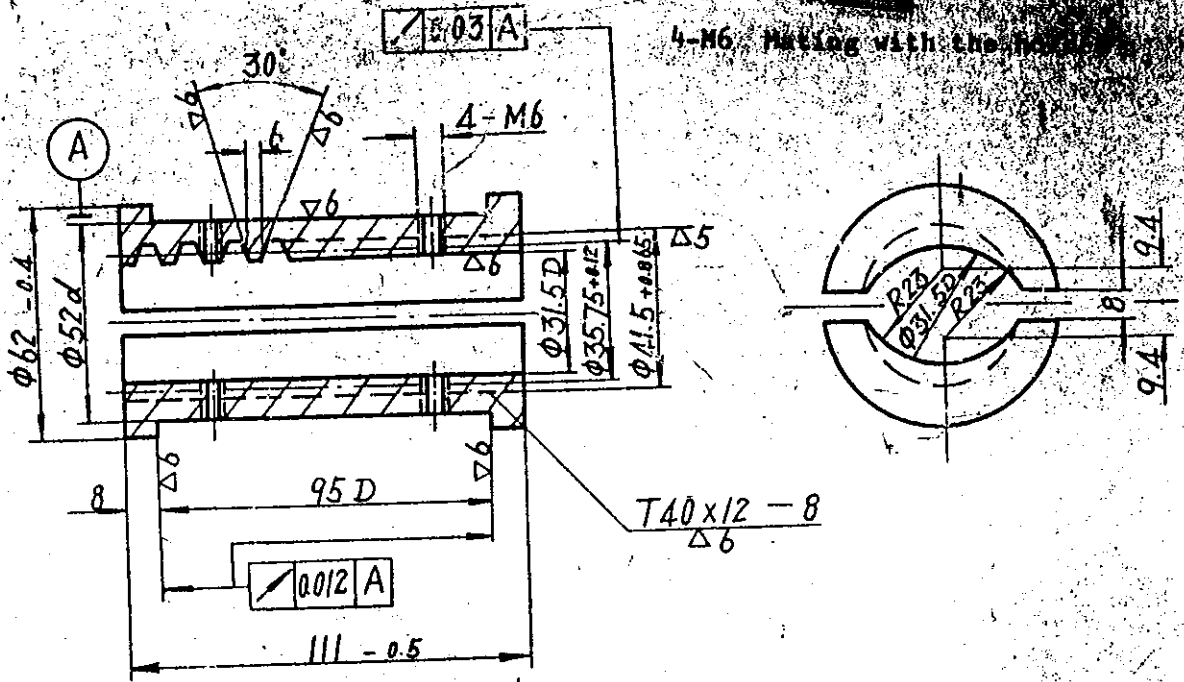
Part No. A 05011 Name: Slide nut Material ZqSn 6-6-3



Type of worm: Archimedes spiral	Axial tooth angle of worm $\alpha_s = 20$
axial module of worm $m_s = 2.5$	No. of teeth of worm wheel $Z_2 = 26$
Starts of worm $Z_1 = 2$	Shifting factor of worm wheel $\xi = 0$
Spiral angle and direction of worm $\lambda = 6^\circ 20' 25''$ R.H.	Precision class 8DC

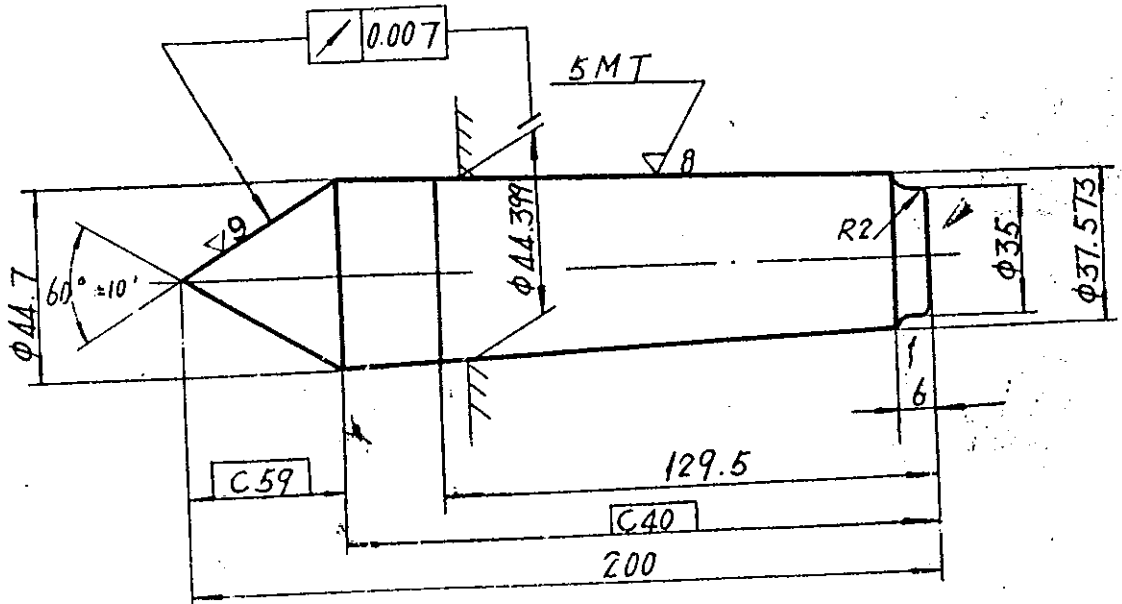
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代号	57-AB-R
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共 61 页	第 58 页

Part No. W06021-R
 Name Worm wheel
 Material ZQSn 6-6-



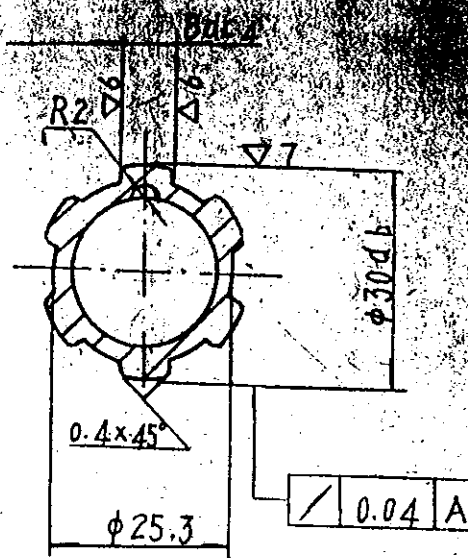
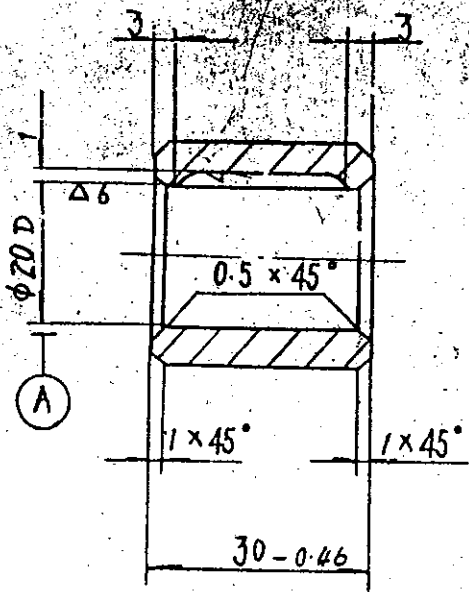
Part No. A06022
 Name Split-nut
 Material ZQSn 6-6-3

Others $\nabla 5$

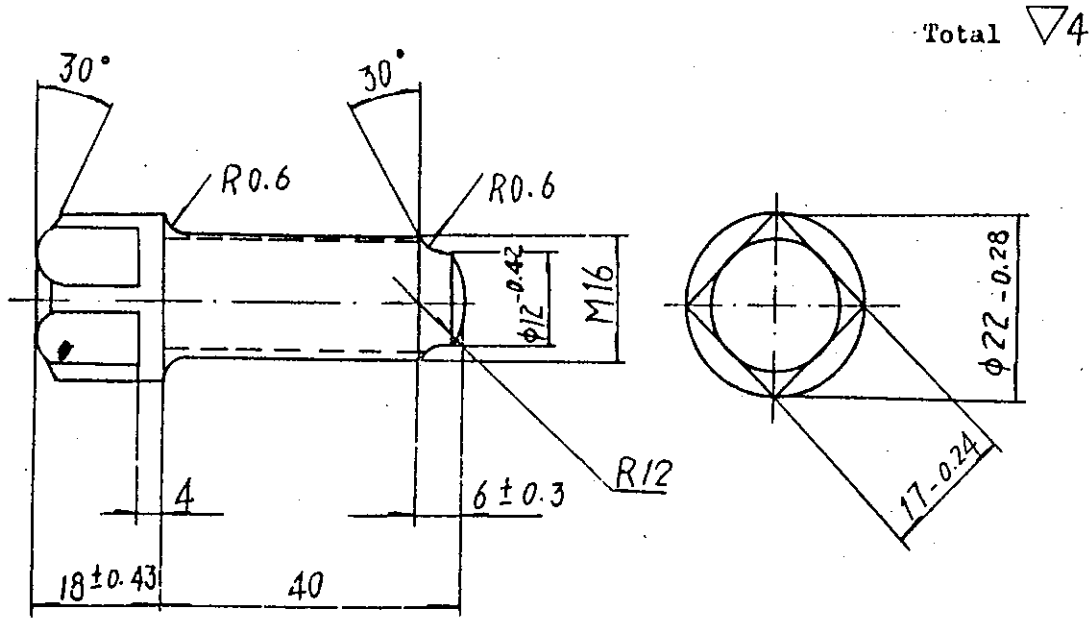


Symbol S77-1
 Size 5MT
 Name Center
 Material T8

产品型号	SY-AB-7
文件代号	共 61 页
日期	第 59 页

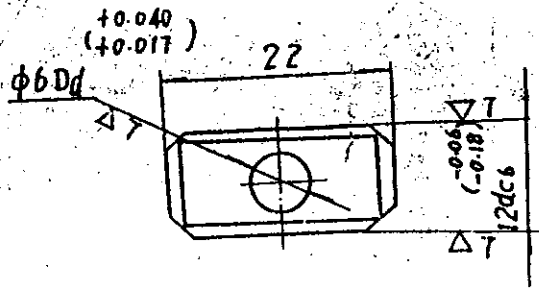


Part No. A08011.
 Name Splined bush
 Material ZqSn 6-6-3



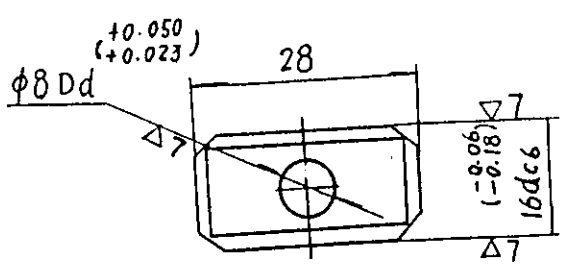
Symbol J22-1
 Size M16 x 40
 Name Screw
 Material 35

产品型号	
文件代号	SY-AB-t
第 60 页	共 61 页



Others $\nabla 4$

Symbol Q99-1
 Size 12
 Name Slide block
 Material HT20-40



Others $\nabla 4$

Symbol Q99-1
 Size 16
 Name Slide block
 Material HT20-40

产品型号		第 61 页
文件代号	S7-AB-7	共 61 页
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Spare Parts

The schedule of spare parts

Serial No.	Part No	Name	Material	Heat Treatment	Unit	Remarks
1	A. 01021/750	leadscrew	y40mn		1	
2	/1000	"	"		1	
3	/1500	"	"		1	
4	/2000	"	"		1	
5	A01024	gear rack	45		2.3 4.6	
6	A01025	"	"		1	0.75M centre distance for (C)62 ⁴⁰ / ₃₀ B TORA ₂ 01025A
7	AB02051	spindle	"	T235 G50	1	
8	A02052	I shaft	"	T235	1	
9	A02053	II shaft	"	"	1	
10	A02054	III shaft	"	"	1	
11	A02055	IV shaft	"	"	1	
12	A02056	V shaft	"	T235 G48	1	
13	A02057	VI shaft	"	T235	1	
14	A02058	IX shaft	"	"	1	
15	A02059	X shaft	"	"	1	
16	A02061	VIII shaft	"		1	
17	A02062	XI shaft	"	G48	1	
18	A02065	XIV shaft	"	"	1	
19	A02081	gear	"	"	1	
20	A02082	"	"	"	1	
21	A02083	"	"	G52	1	

Serial No.	Part No	Name	Material	Heat Treatment	Unit	Remarks
22	A02084	gear	45	G52	1	
23	A02085	"	"	"	1	
24	A02086	"	"	"	1	
25	A02087	"	"	"	1	
26	A02088	"	"	"	1	
27	A02089	"	"	"	1	
28	A02091	"	"	"	1	
29	A02092	"	"	"	1	
30	A02093	"	"	"	1	
31	A02094	"	"	"	1	
32	A02095	"	"	G48	1	
33	A02096	"	"	"	1	
34	A02097	"	"	"	1	
35	A02098	"	"	"	1	
36	A02099	"	"	"	1	
37	A020101	"	"	"	1	
38	A020102	"	"	"	1	
39	A020103	"	"	"	1	
40	A020104	"	"	"	1	
41	A020105	"	"	"	1	
42	A020106	"	"	"	1	
43	A020107	"	"	"	1	
44	A020108	"	"	"	1	

产品型号	文件代号	日期
	SY-48-7	
第 2 页	共 6 页	

Serial No.	Part No	Name	Material	Heat Treatment	Unit	Remarks
45	A02109	gear	45	G48	1	
46	A02111	"	"	"	1	
47	A02114	"	"	"	1	
48	A03005	nut	H715-33		1	
49	A03021	bush	45	local G48	1	
50	A03022	leadscrew	y40mn		1	
51	A04011	nut	ZQSn6-6-3		1	
52	A04031	leadscrew	y40mn		1	
53	A04043	cam	40cr	local G48	1	
54	A04044	pin	20cr	So.9-C59	1	
55	A04046	lever seat	45		1	
56	A04048	ward circle	local G48		1	
57	A04059	bush	20cr	So.9-C59	4	
58	A04061	clutch	40cr	local G48	1	
59	A05011	nut	ZQSn6-6-3		1	
60	A05021	leadscrew	y40mn		1	CY6 $\frac{1}{2}$ 50B for A ₁ 05021
61	A05031	gear	45	gear G48	1	
62	A06021	worm wheel	ZQSn6-6-3		1	
63	A06022	split-nut	"		1	
64	A06051	I shaft	45	T235	1	
65	A06052	II shaft	"	T235 gear G48	1	
66	A06053	III shaft IV shaft	"	T235	1	
67	A06054	IV shaft	"	"	1	

产品型号
号

Serial No.	Part No.	Name	Material	Heat Treatment	Unit	Remarks
68	A06055	V shaft	45	T235	1	
69	A06056	VII shaft	45		1	
70	A06057	VIII shaft	"		1	
71	A06058	IX shaft	"	local G48	1	
72	A06061	gear	"	"	1	
73	A06062	"	"	"	1	
74	A06063	"	Gcr15	y60	1	
75	A06064	"	45	gear G48	1	
76	A06065	"	"	"	2	
77	A06066	"	"	"	4	
78	A06067R	"	"	gear G48	1	
79	A06068R	"	"	"	1	
80	A06069	"	"	"	1	
81	A06071	"	"	face-gear G48	1	
82	A06081	operating shaft	"	T235	1	
83	A06082	rod bush	"		1	
84	A06083	clutch	Gcr15	local G48	1	
85	A06084	"	40cr	local G52	1	
86	A06085	"	45	local G48	1	
87	A06092	interlock pin	"		1	
88	A06107A	connecting bush	"		1	
89	A07031	shaft	"	T235	1	
90	A07032	gear shaft	"	T235 local G42	1	

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日期		
	共 6 页	第 4 页

Serial No	Part No	Name	Material	Heat Treatment	Unit	Remarks
91	A07033	shaft	45	T235	1	
92	A07034	gear shaft	"	gear G42	1	
93	A07035	shaft	"	T235	1	
94	A07036	"	"	"	1	
95	A07037	"	"	"	1	
96	A07038	gear shaft	"	gear G42	1	
97	A07039	shaft	"	T235	1	
98	A07061	gear	"	gear G42	1	
99	A07062	"	"	"	1	
100	A07063	"	"	"	1	
101	A07064	"	"	"	1	
102	A07065	"	"	"	1	
103	A07066	"	"	"	2	
104	A07067	"	"	"	1	
105	A07068	"	"	"	1	
106	A07069	"	"	"	1	
107	A07071	"	"	"	1	
108	A07072	"	"	"	1	
109	A07073	"	"	"	1	
110	A07074	"	"	"	1	
111	A07075	"	"	"	1	
112	A07076	"	"	"	1	
113	A07077	"	"	"	1	

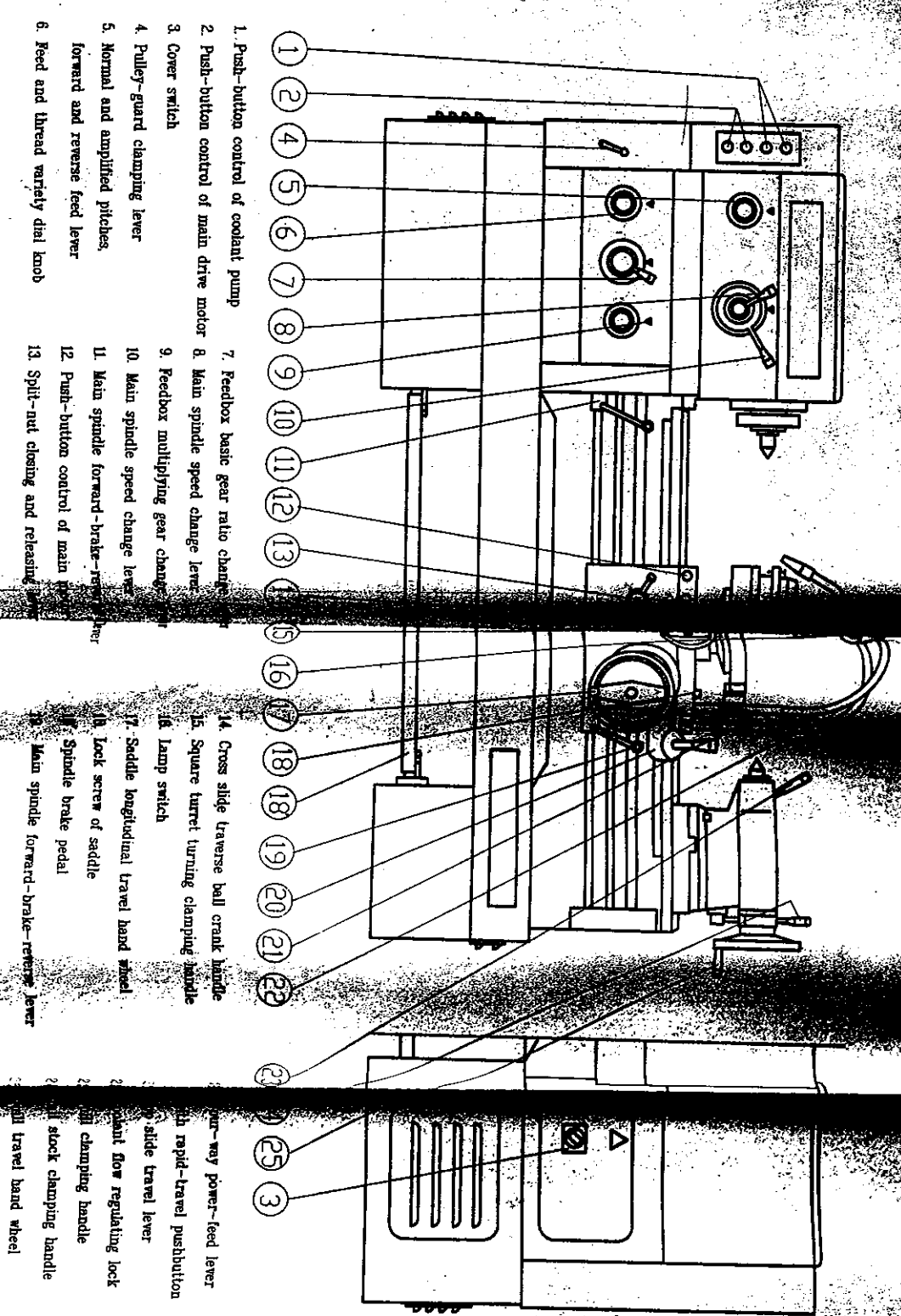
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4. Emergency brake

To prevent the situation from getting worse and worse at the time of emergency circumstance occurrence, step down the pedal which was build between the legs.

The main power was cut off once the pedal begin step-downed and the brake torque was imposed by the brake hand to the V-belt thus the brake of the main motor and spindle was quickly realized. After completion of above-mentioned operation.

If the forward-backward-stop lever of the spindle is in the original position (upward for spindle forward rotation, downward for reversed rotation), then the limited switch mounted on the vertical spindle with stop the machine's restart , to prevent the accident from happening. When restart is needed, set the above-mentioned lever to the spindle-stop position and operate the start pushbutton of the main motor.



1. Push-button control of coolant pump
2. Push-button control of main drive motor
3. Cover switch
4. Pulley-guard clamping lever
5. Normal and amplified pitches forward and reverse feed lever
6. Feed and thread variety dial knob
7. Feedbox basic gear ratio change
8. Main spindle speed change lever
9. Feedbox multiplying gear change
10. Main spindle speed change lever
11. Main spindle forward-brake-reverse lever
12. Push-button control of main spindle
13. Split-nut closing and releasing lever
14. Cross slide traverse ball crank handle
15. Square turret turning clamping handle
16. Lamp switch
17. Saddle longitudinal travel hand wheel
18. Lock screw of saddle
19. Spindle brake pedal
20. Main spindle forward-brake-reverse lever
21. Four-way power-feed lever
22. Rapid-travel pushbutton
23. Side travel lever
24. Coolant flow regulating lock
25. Clamping handle
26. Stock clamping handle
27. Travel hand wheel

Fig 2 Operating element and lever locations

VI. ELECTRICAL SYSTEM

The principle of electrical system is shown in page 6-3. The electric wire diagram is shown in page 6-4. The electric equipments diagram is shown in page 6-5 and the electric equipments list are shown in page 6-6.

For adapting to the different power systems of various countries and regions, the machine can be provided optionally with electrical equipments in AC frequency of 50HZ or 60HZ, in control voltage of 110v and in main voltage of 220V, 380V, 420V, or 440V, 600V, illuminator voltage of 24V, and in main motor power of 10HP, 15HP or 20HP. It is necessary for our endusers to make sure that the frequency and the voltage given or rating plate agree with the local power system.

Fuses are not provided with this machine. They can be mounted on the leading power line by our endusers according to the data on the rating plate.

Both power line and protective earth line should enter the machine through the cable gland on the left side of the front cabinet leg, since the wiring board is also placed to the left of its rear window. An enriching wire is to be let out from side hole and tightened on the screw connecting (PE) to the ground.

After closing the main switch QS, the pilot lamp HL1 and HL2 in green pushbuttons SB2 and SB3 of main motor M2 will light up, it shows that the circuit is being connected and that the main motor is being started. By pressing down the start—button of main motor, the pilot lamps will go out, it shows the completed and the main motor is being started. By pressing down

the red pushbutton SB4 which serve to stop the main motor

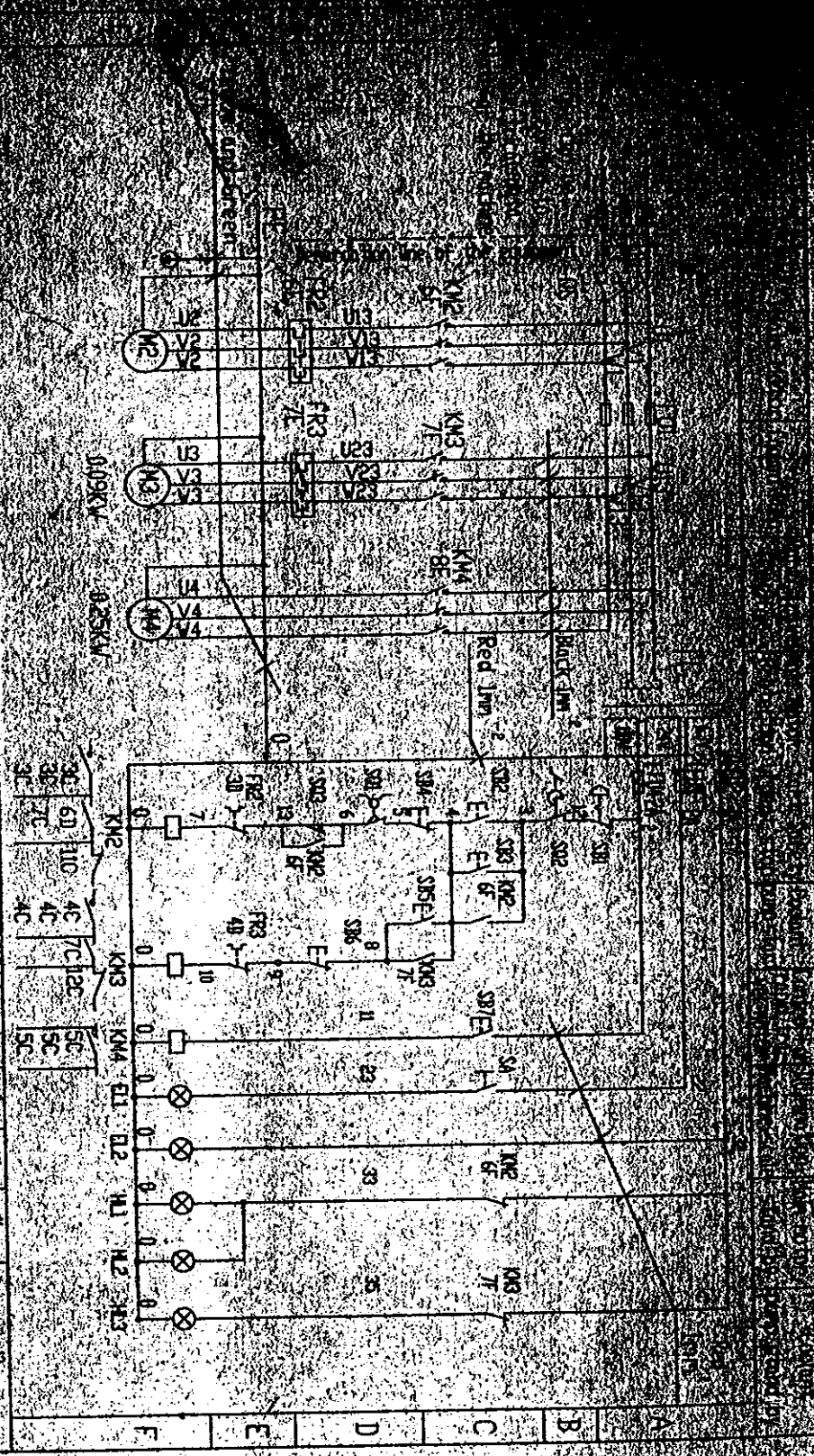
After starting the main motor, the pilot lamp HL3 in green start button SB5 of coolant pump will light up, pressing down this button may start the coolant pump. Once the main motor is stopped, the coolant pump will stop automatically.

A protective switch SQ is built in the belt cover, when opening the cover, the main motor can't be started. An urgent stop-pushbutton (SB1) can cut off electric circuitry and can stop the machine. After removing trouble, turn this button in the direction the black arrow indicate to 30°, then the machine can be restarted.

After the electric power is being connected, the rapid travel motor M4 is controlled by black pushbutton SB7 and the work lamp EL1 is controlled by switch K on lamp socket.

A hanger hole for the naked lock is also provided with the power switch of the machine. Various naked locks can be equipped at the customers choice .

Special tools for opening the electrical equipment cabinet are available in accessory box.

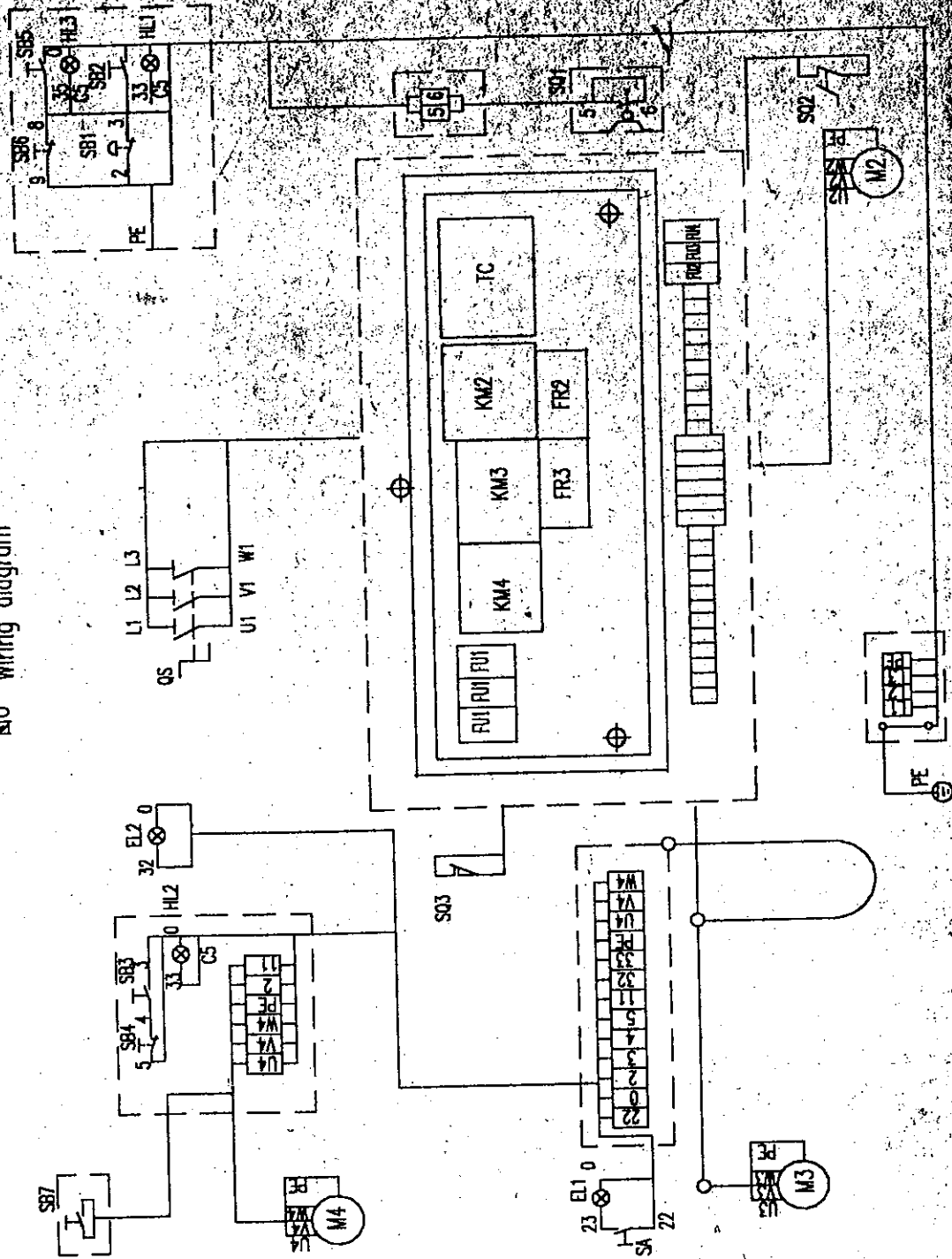


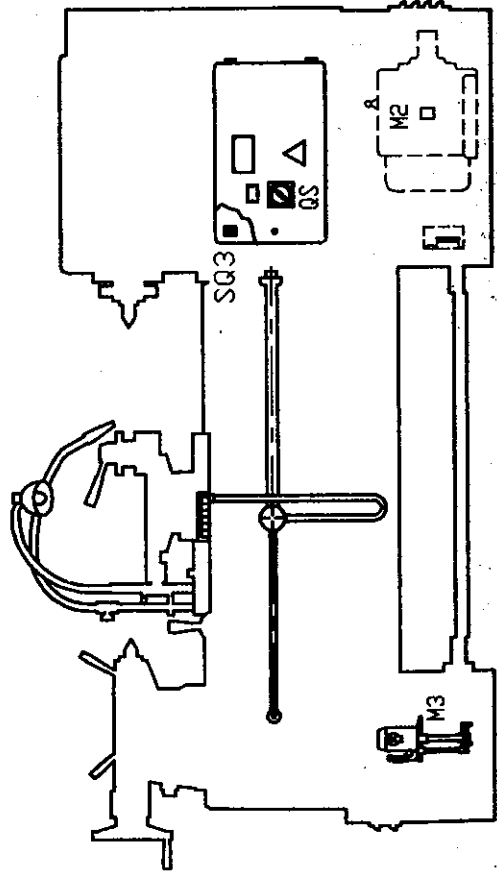
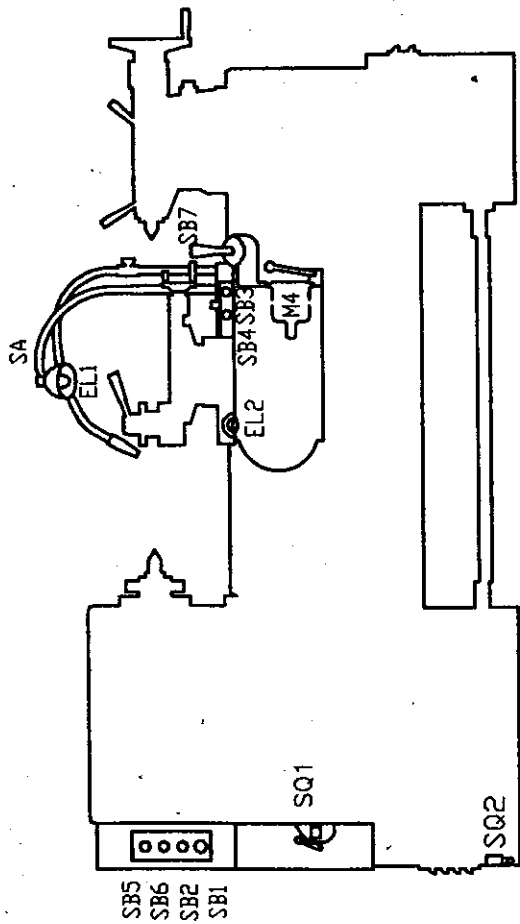
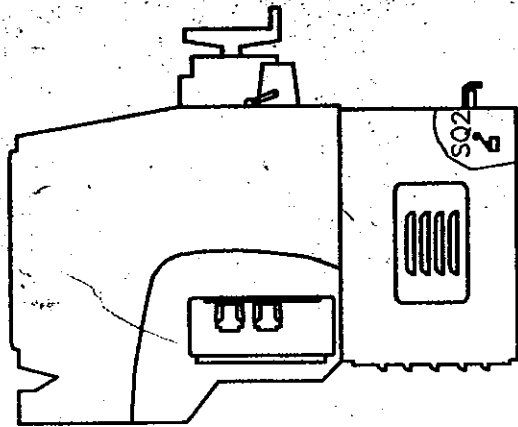
V	FR1	FU1	FR2	FR3	FU2	FR3	FU3	B			FR2	FR3	FU4
								1	2	3			
-220V	0.58A	10A	39A	0.58A	10A	0.58A	10A						
-380V	0.32A	6A	22.5A	0.32A	6A	0.32A	6A						
-420V	0.32A	6A	20A	0.32A	6A	0.32A	6A						
-440V	0.32A	6A	19.6A	0.32A	6A	0.32A	6A						
-600V	9.7A	4A	14.3A	0.2A	4A	0.2A	4A						

Note: the value of thermal relay is the reference value, using the marked value on the data plate as standard. Users must take care of this!

The Diagram of Electric Circuit

图6 Wiring diagram





Installation diagram

POWER 3~50HZ<60HZ>